

High power target and beam dump system for BigRIPS fragment separator

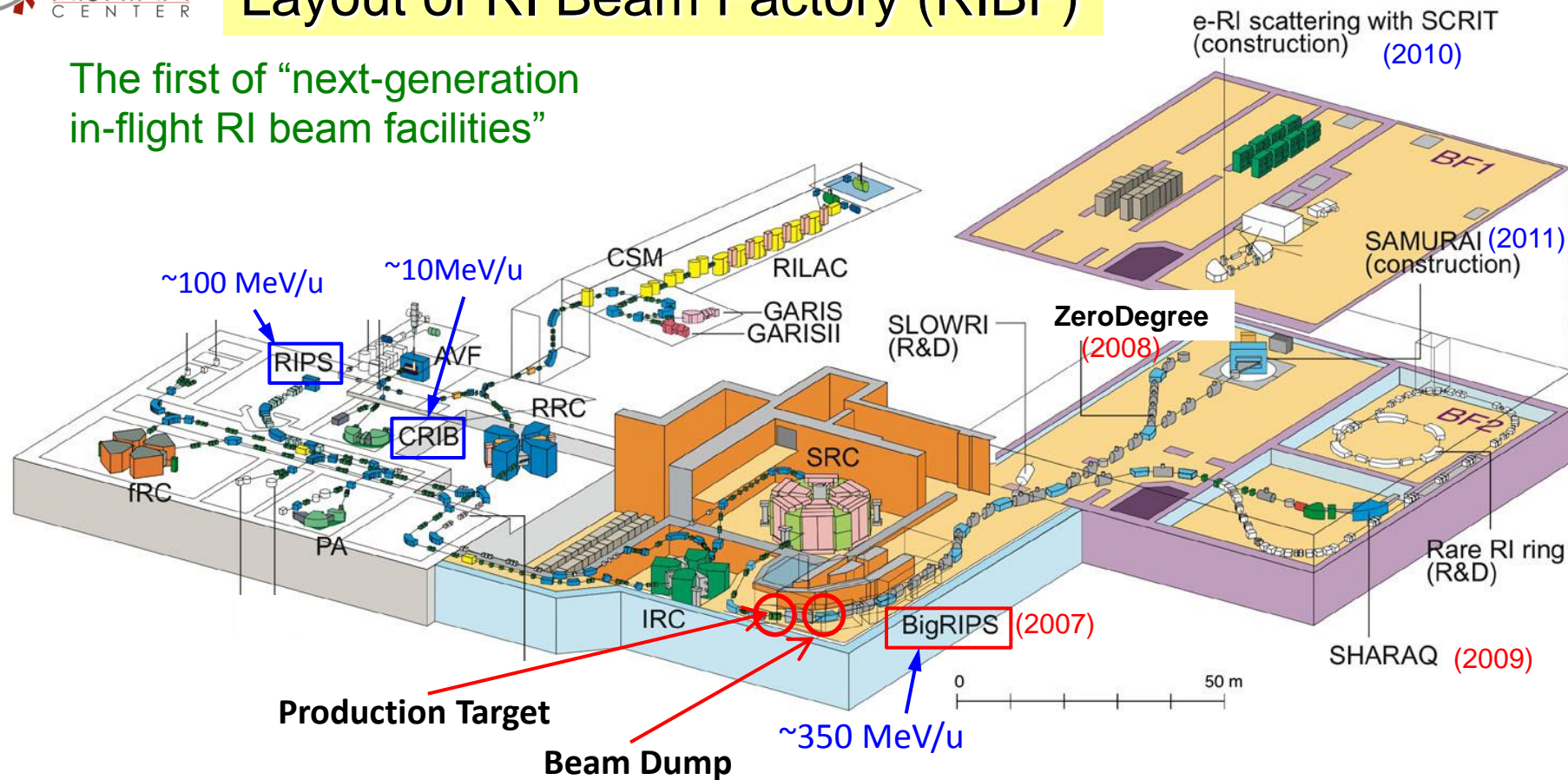
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BigRIPS Team

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Layout of RI Beam Factory (RIBF)

The first of “next-generation in-flight RI beam facilities”



- RIBF accelerator system consists of a linac and four cyclotrons. **RRC, fRC, IRC, SRC**
- Maximum energy is ~ 350 MeV/u for heavy ions up to U ions.
- Goal beam intensity is $1 \text{ p}\mu\text{A}$ (6×10^{12} particles/sec) **Max. beam power 83 kW**

Available Beam intensity: Beam energy = 345 MeV/n (*250 MeV/n)

$^{14}\text{N}^*$	400pA (1.4kW)	^{48}Ca	415pA (6.9kW)	^{124}Xe	27pA (1.2kW)
^{18}O	1000pA (6.2kW)	^{70}Zn	100pA (2.4kW)	^{238}U	12pA (1.0kW)

Beam Spot and Power Density

Beam Power (^{238}U 345MeV/n, $1\mu\text{A}=83\text{kW}$) is dissipated in a **target** and a **beam dump**.

Target

Beam Spot Size:

$\phi \sim 1\text{mm}$ (fwhm)

Target Thickness :

Optimum thickness $\sim 1/3$ of the Range.

Material:

Be, C, W, Pb, etc.

Melt. Point 1284, 3600, 3382, 328 °C

Beam Power in Target (Be 1/3 Range)

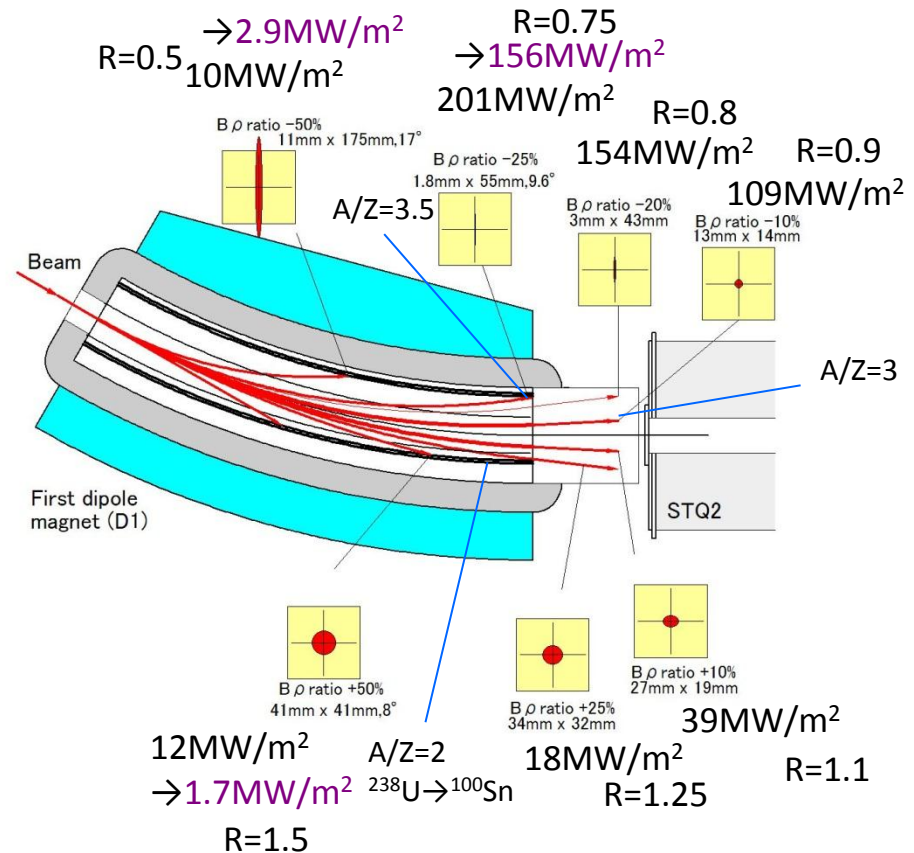
Prim. Beam	$^{238}\text{U} \sim ^{48}\text{Ca} \sim ^{12}\text{C}$	$1\mu\text{A}$
Trg. Thick	4.4 ~ 17.2 ~ 47.9 [mm]	Be
Trg. ΔE	19.7 ~ 3.2 ~ 0.9 [kW/ $1\mu\text{A}$]	
	in $\phi 1\text{mm}$	25.1 ~ 4.1 ~ 1.1 [GW/ m^2]
	in volume	5.7 ~ 0.2 ~ 0.02 [kW/ mm^3]

Beam Dump

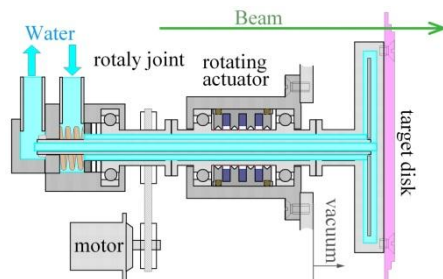
placed inside and exit portion of D1 magnet

Beam Spot Size, Power Density

varied as RI beam setting. $R = B\rho_{\text{beam}} / B\rho_{\text{separator}}$
for the case of ^{238}U 345MeV/n with 4.4mm Be target,



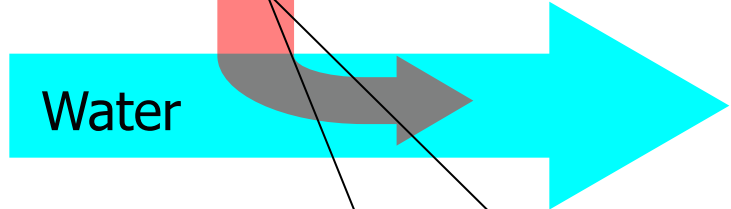
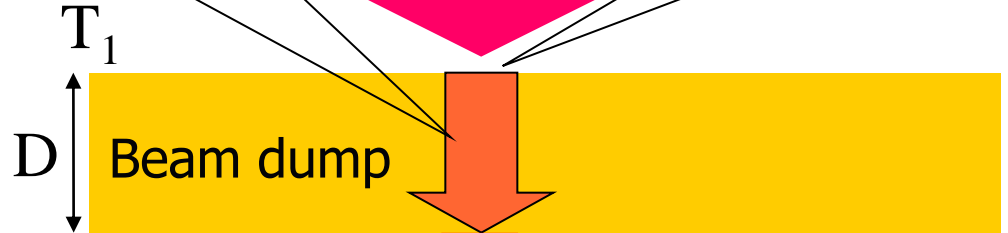
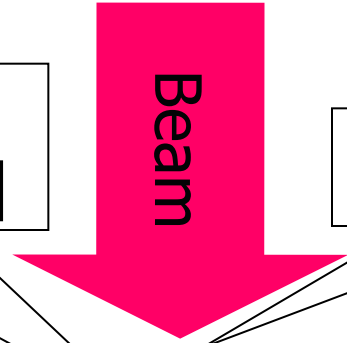
Rotating wheel target with water cooling



Stationary system with water cooling

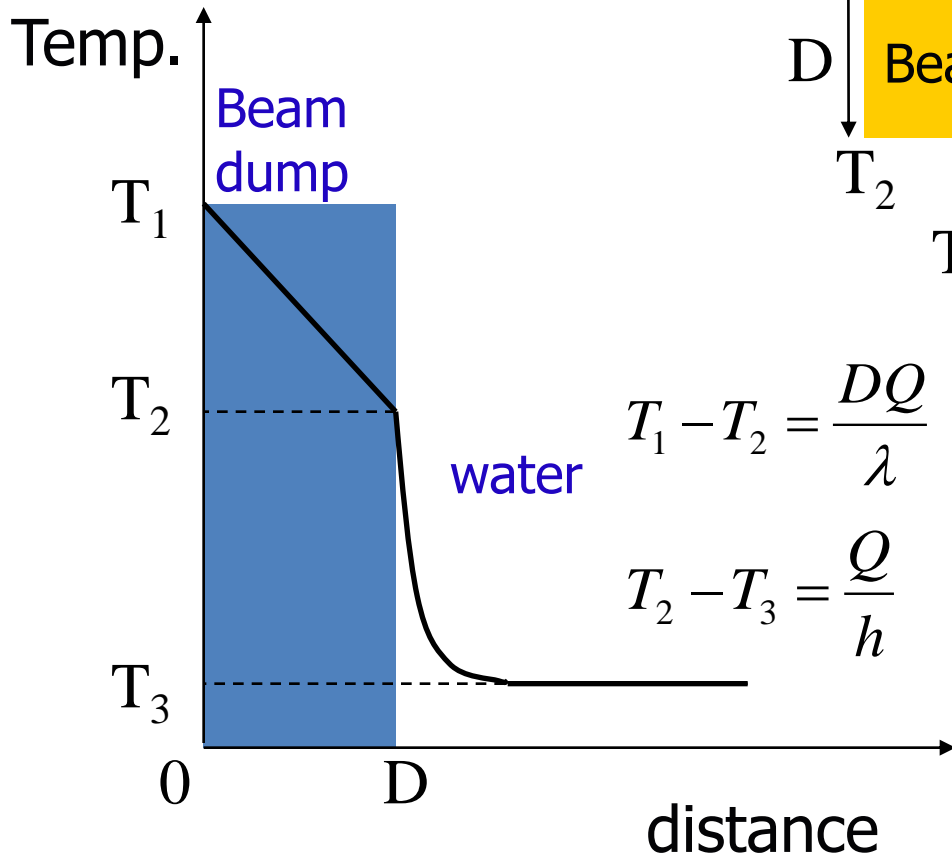
Cooling by Water flow

Thermal conduct. λ [W/m K] Heat Q [W/m²]



Heat transfer coeff. h [W/m²K]

Heat transfer coefficient: $h \uparrow$
 Thermal conductivity: $\lambda \uparrow$
 Cu-alloy
 Distance: $D \downarrow$ tilted wall

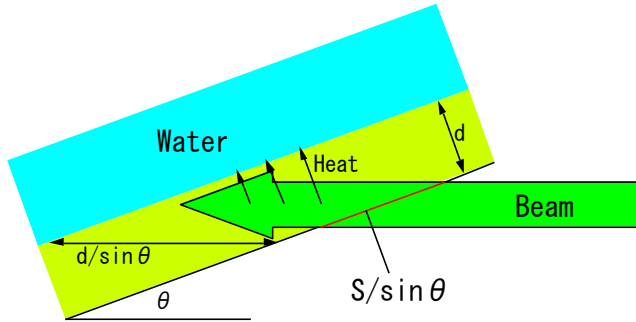
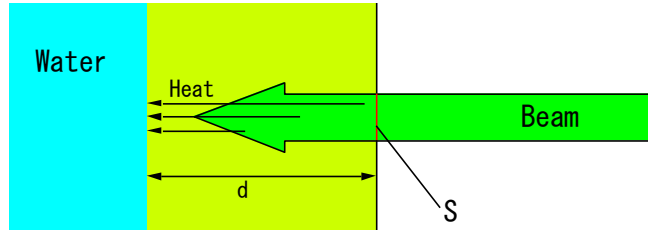


$$T_1 - T_2 = \frac{DQ}{\lambda}$$

$$T_2 - T_3 = \frac{Q}{h}$$

Highly efficient method of water cooling

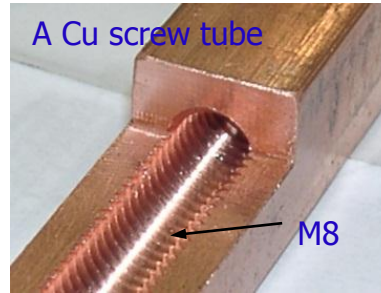
• Tilted Wall



Reduces Power density
 Prolongs effective length
 by $1/\sin\theta$
 $\sin 10^\circ = 0.17$
 $\sin 6^\circ = 0.1$

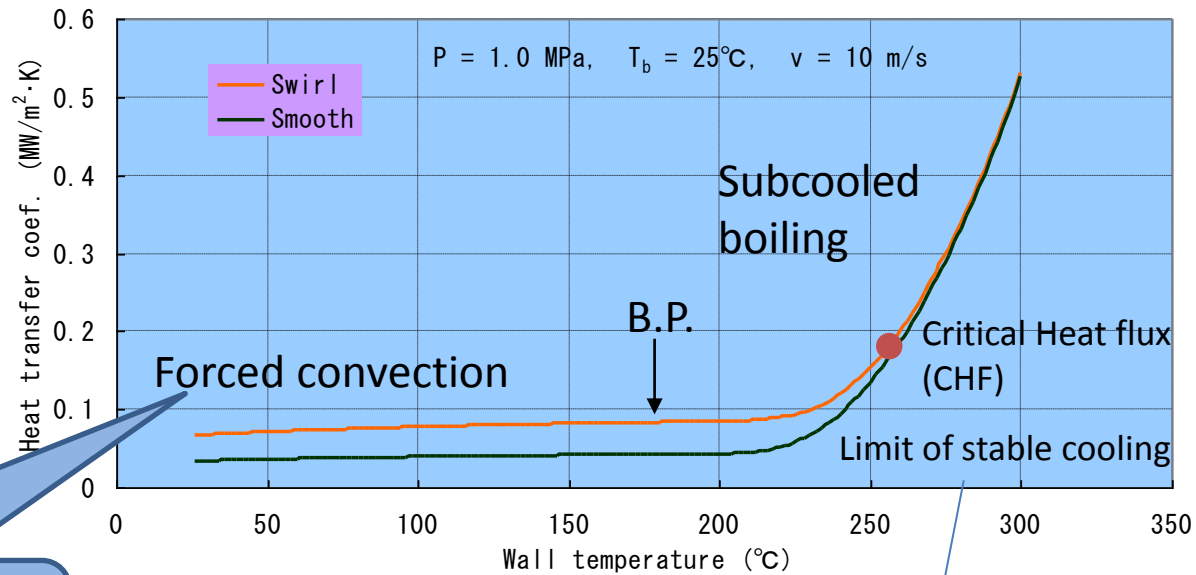
• $h \sim Re^{0.8} Pr^{0.8} \sim v^{0.8}$
 v: flow velocity → use high velocity

• Cooling tubes with high heat transfer coefficient



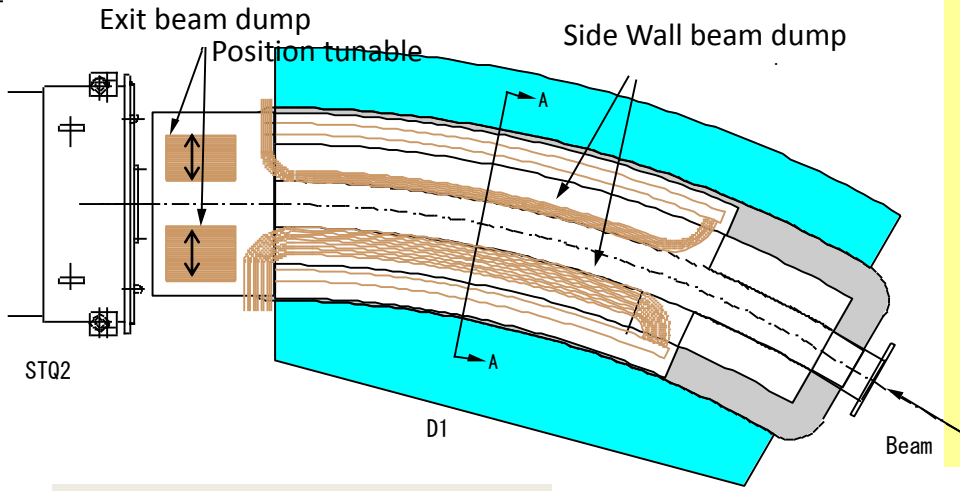
Heat transfer coefficient by JAERI formula

J. Boscary et al. *Fusion Engineering and Design* 43 (1998) 147



Use of highly pressurized water: High boiling point
 1 MPa 180°C

High-power water-cooled beam dump for BigRIPS using swirl tubes and screw tubes (maximum beam power ~100 kW)



1) The side-walls of first-dipole gap

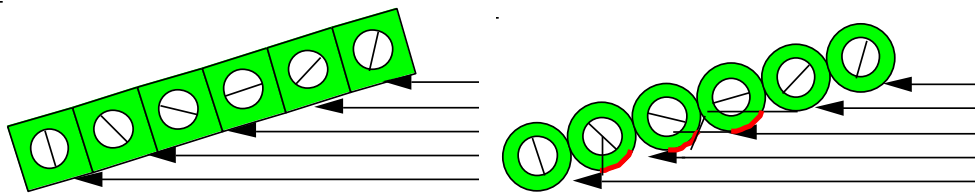
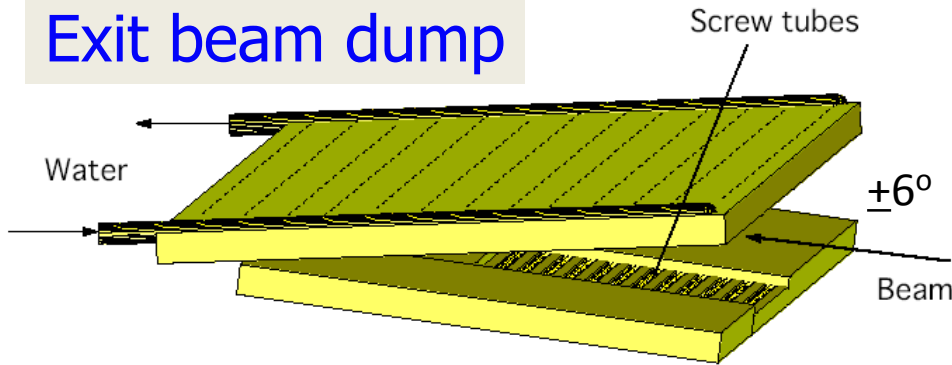
Inside: A screw-tube (Square shape)
OF-Cu $14 \times 14 \text{ mm}^2$, $\backslash 8 \text{ mm}$, $\pm 20^\circ$

Outside: A swirl-tube (Circular shape)
Cu-Ag alloy $\backslash 14 \text{ mm} \times \backslash 8 \text{ mm}$

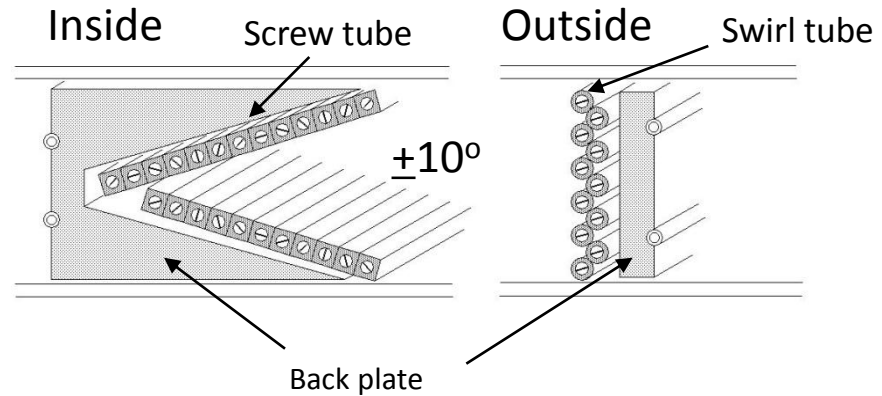
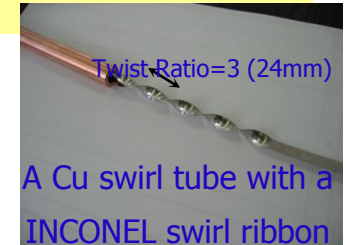
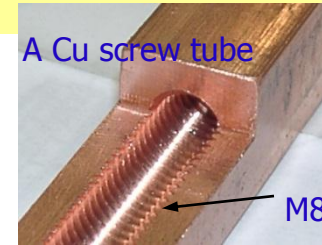
2) The exit of first dipole

A V-shaped screw-tube beam stopper
Cu-Cr-Zr Alloy M8 screw, 3mm Wall thickness
 $\pm 6^\circ$

Exit beam dump

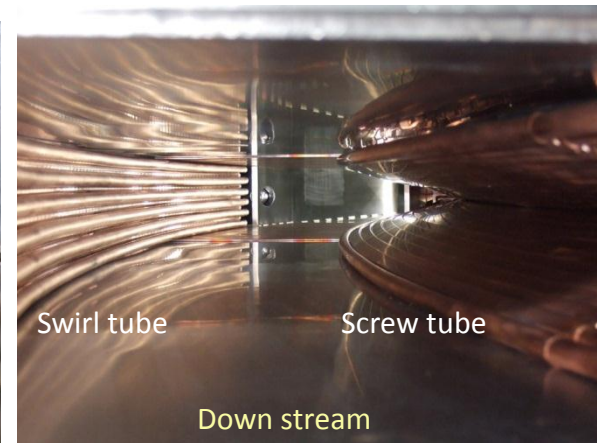
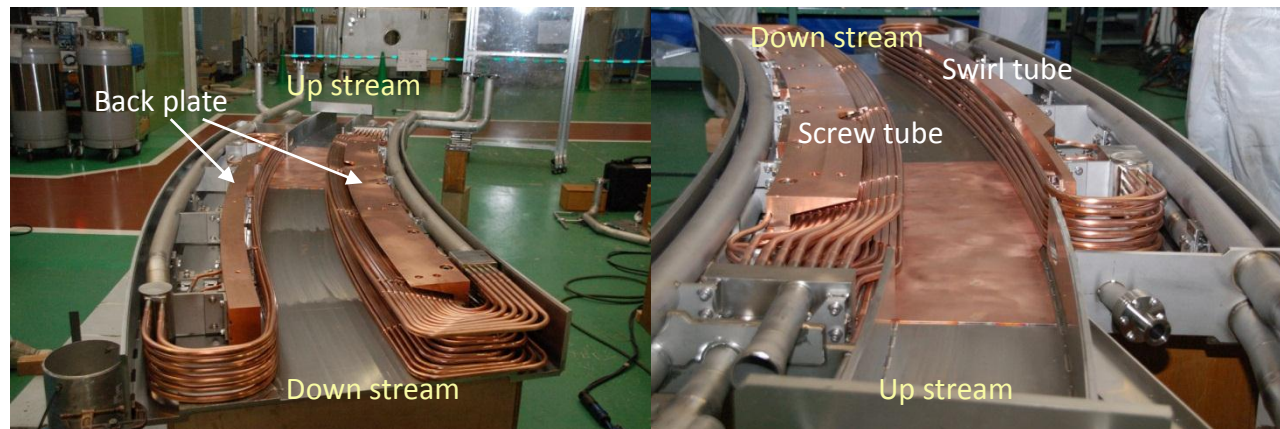


Curved surface suffers high heat flux.

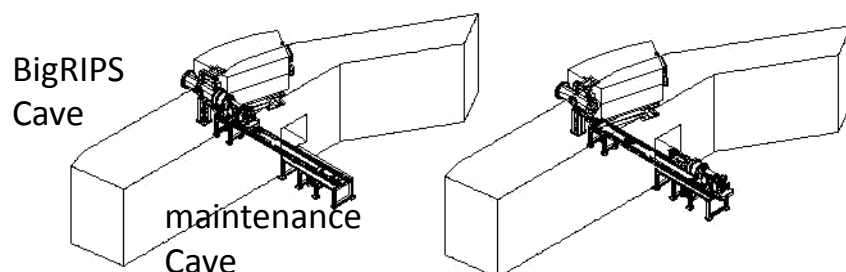
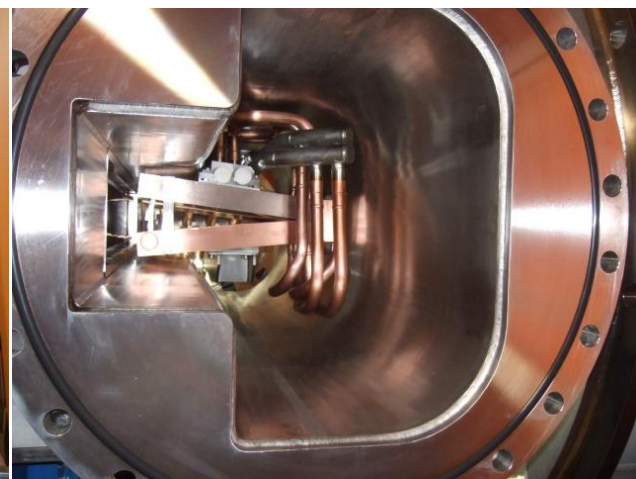


Side-wall beam dump

Side-Wall Beam Dump



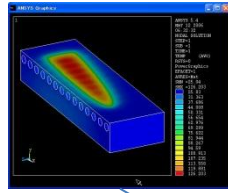
Exit Beam Dump



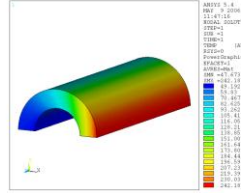
Projected Beam Power Density and ANSYS Simulation

Exit-Dump
Screw tube: M8 screw
3mm Wall thickness,
14mm sep.
material Cu-Cr-Zr alloy
($\lambda=351\text{W/mK}$).

$T_{\max} = 126^{\circ}\text{C}$



Surface: 242°C
Water side: 160°C

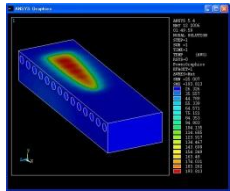


Outer side Dump
Swirl tube: Swirl pitch 3
 $\phi(\text{out})=14\text{ mm}$, $\phi(\text{in})=8\text{ mm}$;
material Cu-Ag alloy
($\lambda=385\text{W/mK}$).

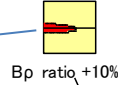
Water conditions:
flow speed= 10 m/s ;
pressure= 1 MPa ;
(boiling temp.= 180°C)

Inner side Dump
Screw tube: M8 screw
 $14\times 14\text{ mm}$ square
material OF-Cu
($\lambda=391\text{ W/mK}$).

$T_{\max} = 192^{\circ}\text{C}$



7.9 MW/m^2



Bp ratio +10%

4.4 MW/m^2



Bp ratio +25%

6.2 MW/m^2



Bp ratio +50%

STQ2

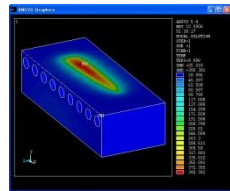
Exit Beam Dump

Side Wall Beam Dump

D1

Beam

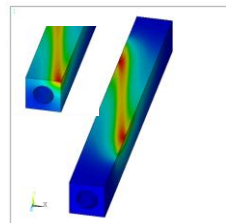
$T_{\max} = 394^{\circ}\text{C}$



22.5 MW/m^2 20 MW/m^2

Bp ratio -10% Bp ratio -20%

45.6 MW/m^2

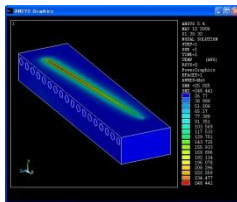


Bp ratio -25%

1.8 MW/m^2

Bp ratio -50%

$T_{\max} = 248^{\circ}\text{C}$



Surface: 369°C
Water side: 154°C



Heating the prototype beam dump by a 1.5 kW CO₂-laser beam

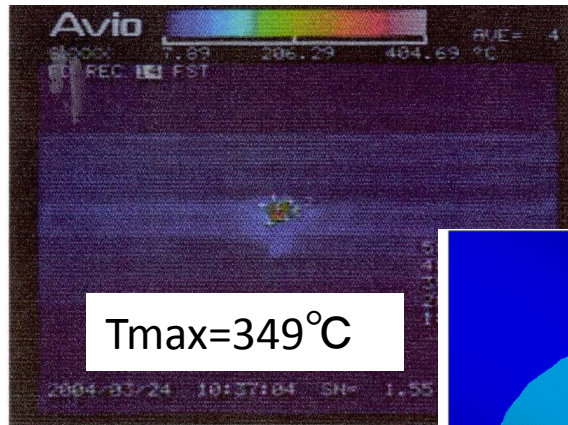
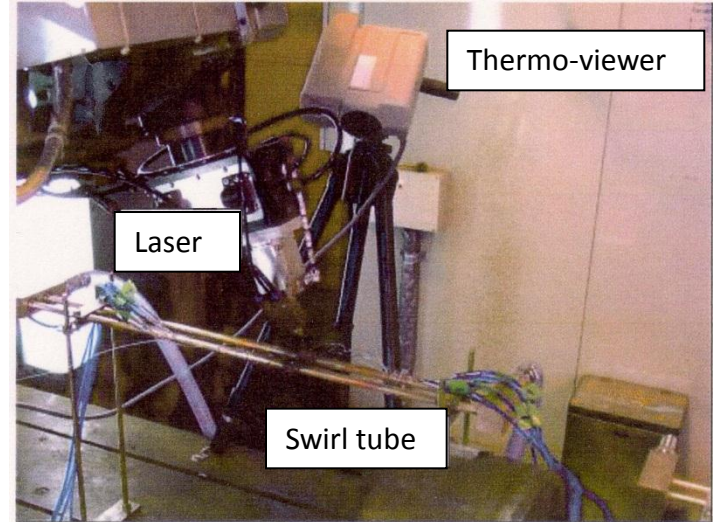
We have examined the cooling capability of a swirl tube with irradiating an expected heat density and spot size, up to 70 MW/m² and 4 mm ϕ .

Swirl tube: Cu-Cr alloy

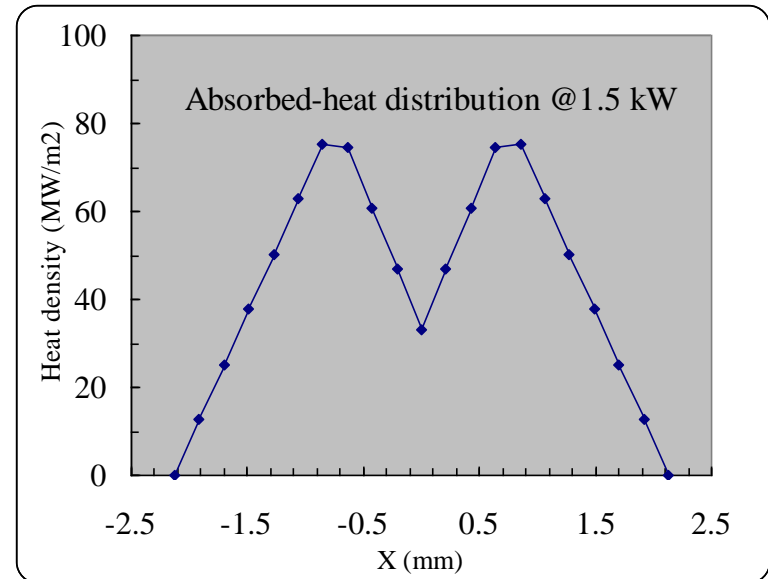
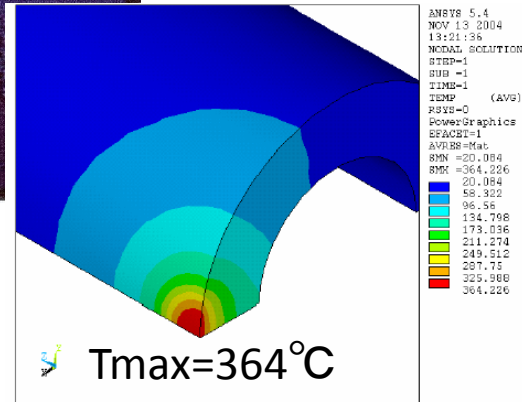
outer 14 mm ϕ , inner 8mm ϕ

Swirl ribbon: Inconel, pitch 24mm/180 $^{\circ}$

Water: 12m/s, 1 MPa



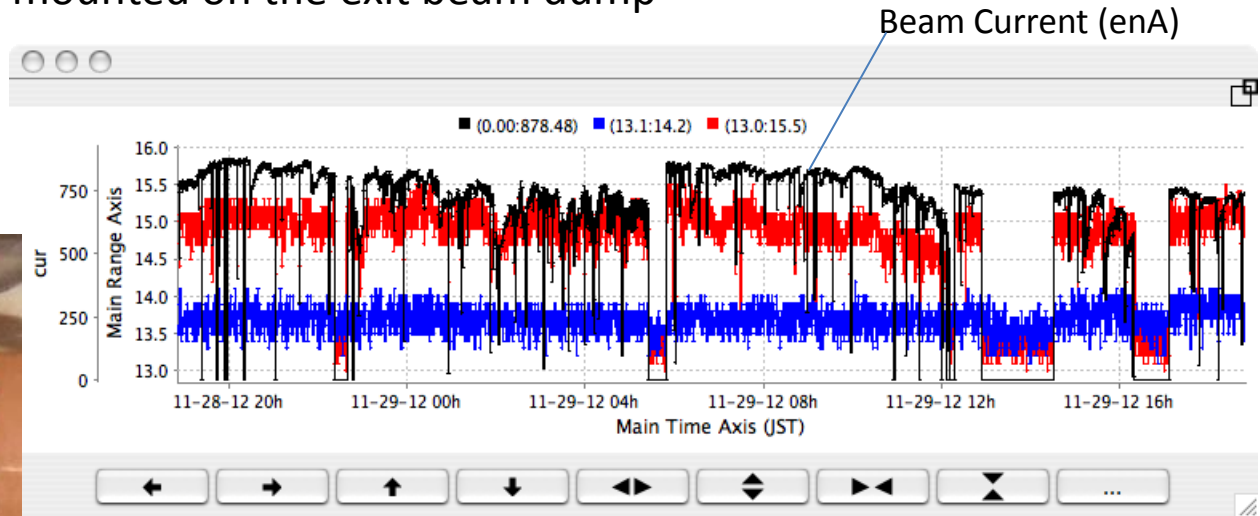
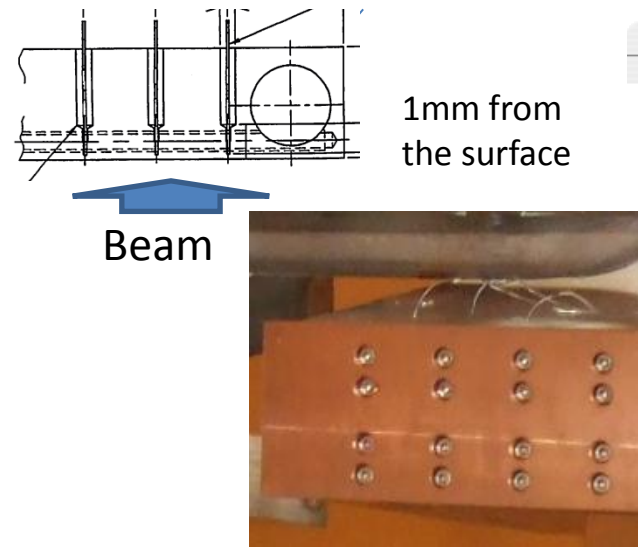
ANSYS calculation reproduces the temperature distribution well.



Beam Dump Temperature for ^{238}U 345MeV/n 8.3pA

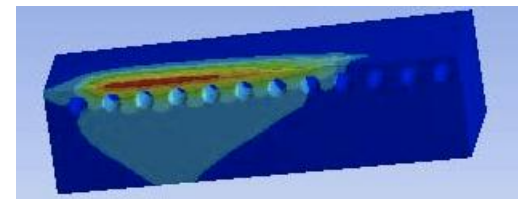
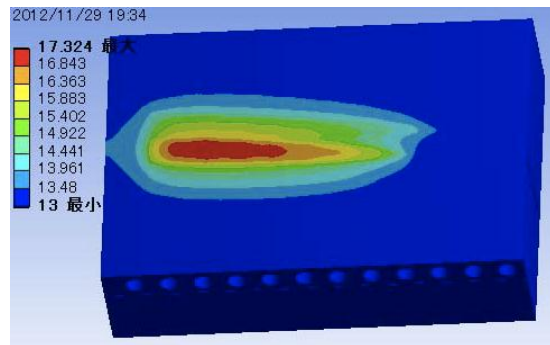
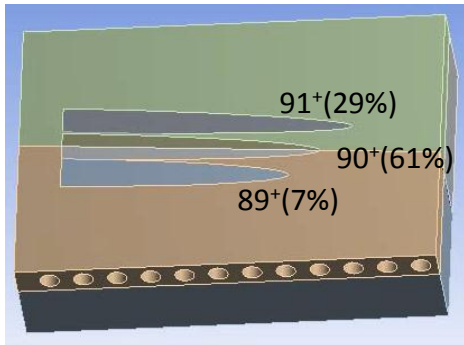
Exit-Dump is operated with water of 13°C, 0.7MPa, and 2.6m/s. (Design: 1MPa, 10m/s)

Thermo-couples mounted on the exit beam dump



Estimated beam spot at dump
Heat load : 522W

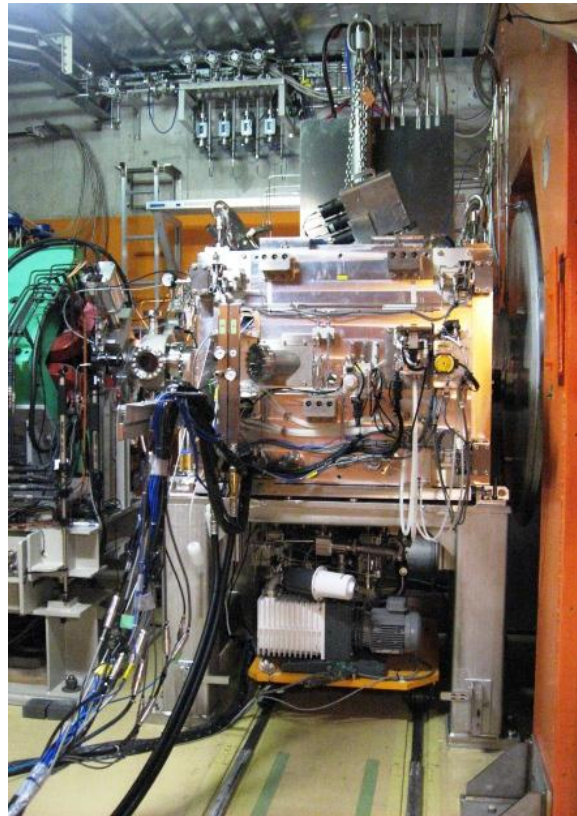
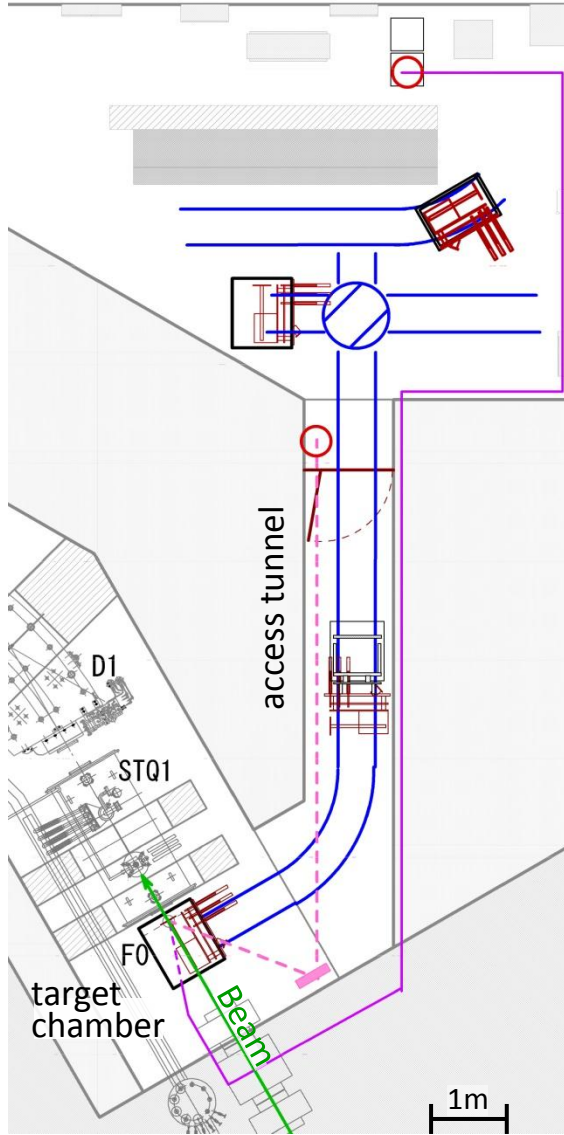
Temperature increase $15.1 - 13.6 = 1.5 \text{ }^\circ\text{C}$



ANSYS simulation: Temperature increase $15.0 - 13.0 = 2 \text{ }^\circ\text{C}$ (not bad, although large ambiguity)

BigRIPS Target System

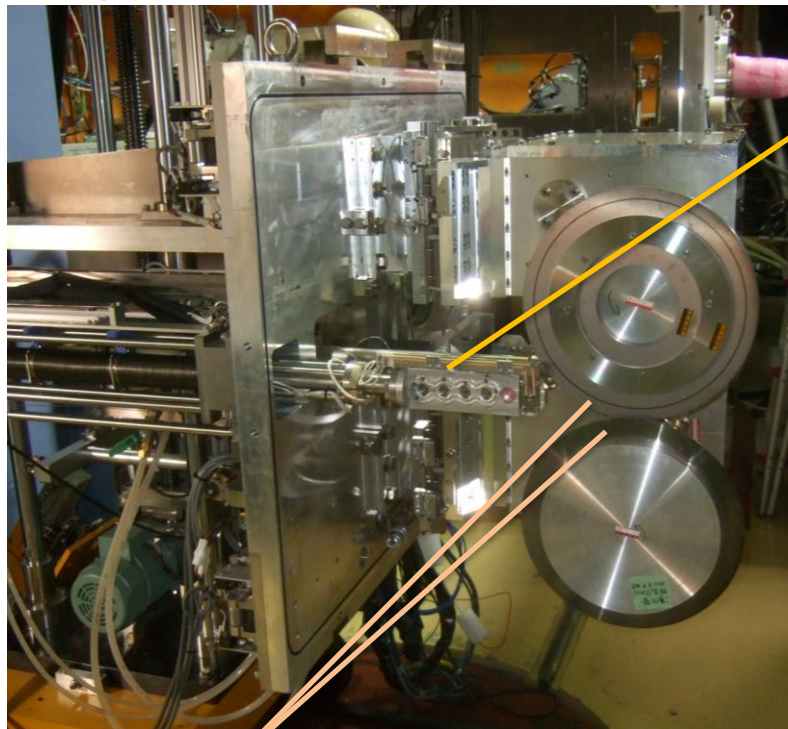
- Two rotating target units and one target ladder (fixed target) are mounted on the side flange.
- The side flange can be carried out by the maintenance cart for maintenances.



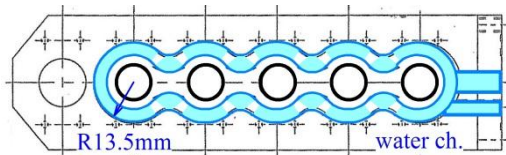
Rotating target

Target ladder (fixed target)

Ladder target and rotating target



Target ladder (fixed target)



The water way is cut in the ladder.

- *Diameter : ~ 20 mm
- *Thickness : 1 ~ 20, ~ 60 mm

Ladder target : for Low-power beam



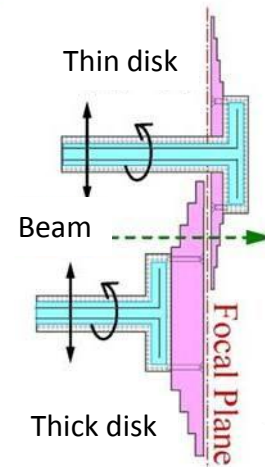
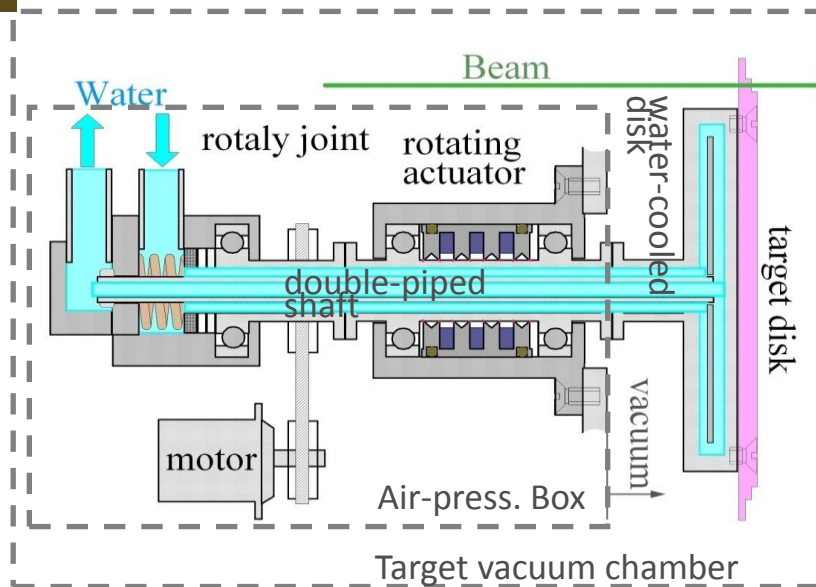
Taper-shape targets are utilized for better thermal contact.

Rotating target

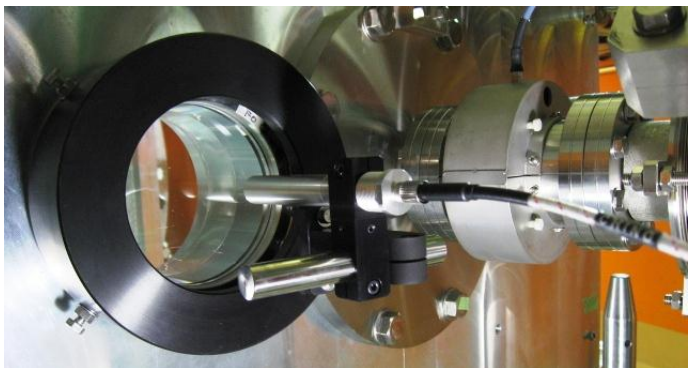
Disk target : for High-power beam

- *Size : $\phi 30\text{cm}$
- *Material : Be, W
- *Step shaped edge
20,15,10 mm thick for N, Ca, Ar beams
10, 7, 5 mm thick for Kr, Xe, U beams

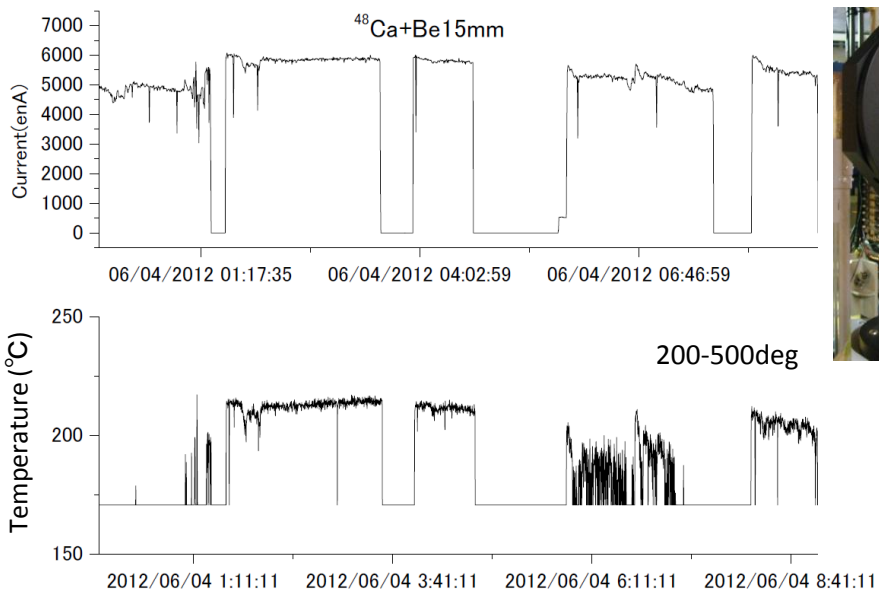
← Be : 20,15,10 mm thick



(1) Infrared Fiber Scope

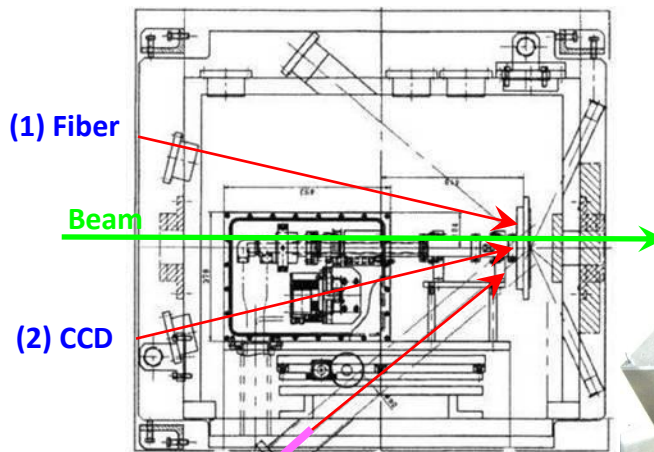


Sapphire view port & Lenz unit mounted on the Target chamber

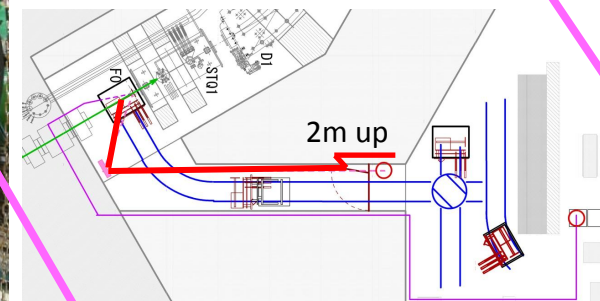
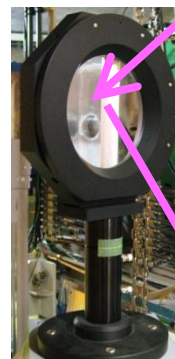


Spot temperature only
 Can be used as on-line monitor
 $T > 200$ deg.

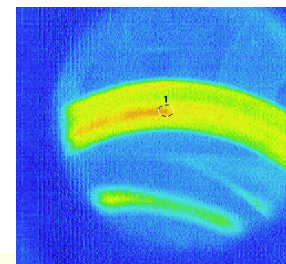
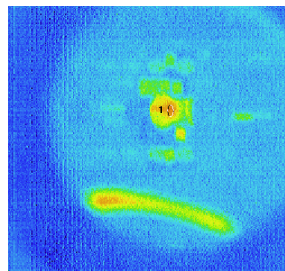
Target chamber (upper view)



(3) IR, Telescope

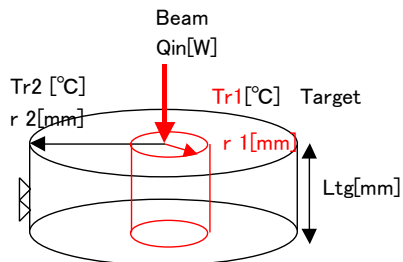


12m distance



(2) IR thermal image camera

((Cylindrical model)) analytical model



$$Tr1 : \text{Beam Spot Temp.} \\ = Tr2 + Q_{in} \cdot \ln(r2/r1) / (2\pi\kappa Ltg) \\ Q_{in} = I_{beam} \cdot dE \\ \propto dE / Ltg$$

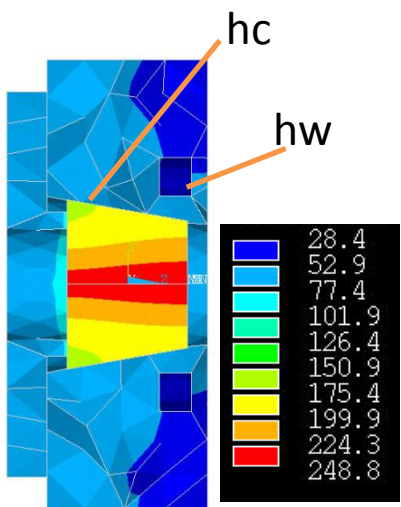
ANSYS calculation

Modeling: whole ladder

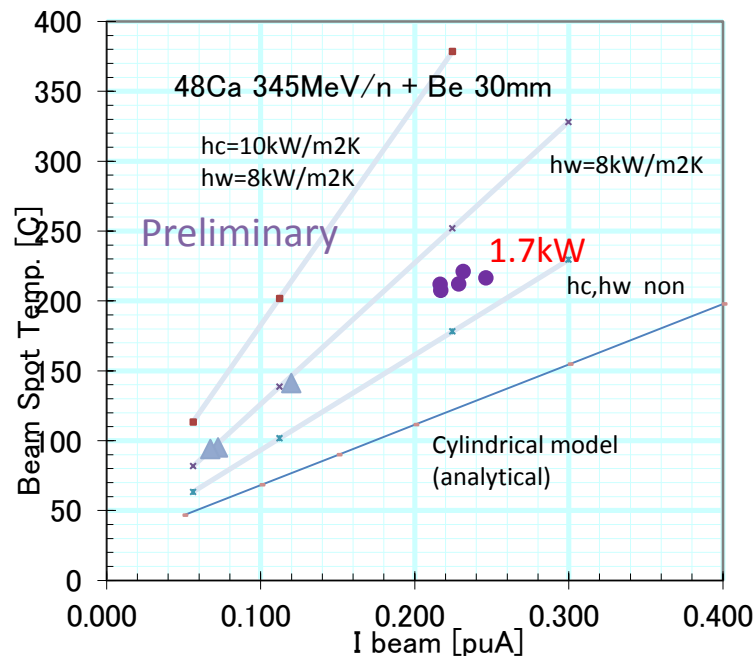
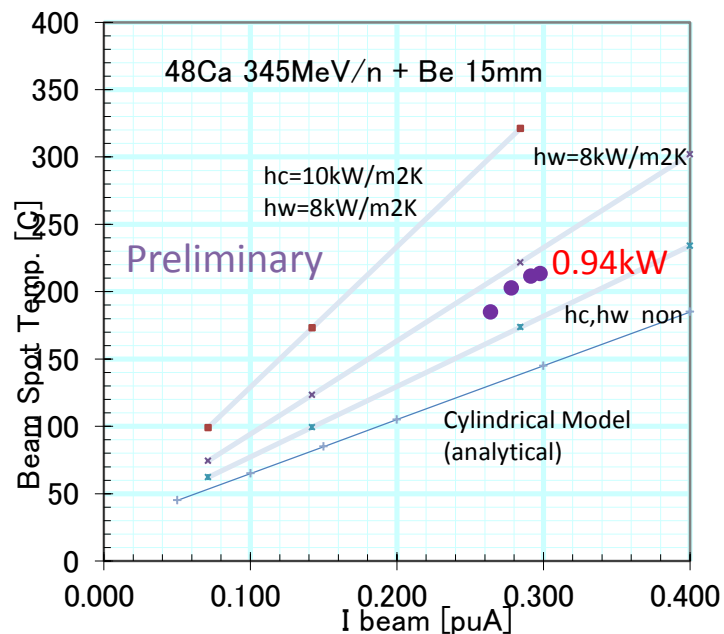
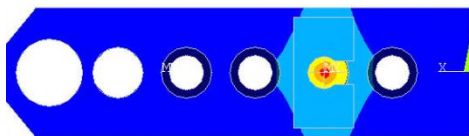
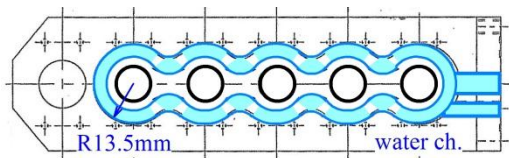
Heat transfer coefficient:

water-ladder: hw turbulence flow 1.5m/s 8kW/m²K

Ladder-target:hc typical CPU Heat sink 10kW/m²K



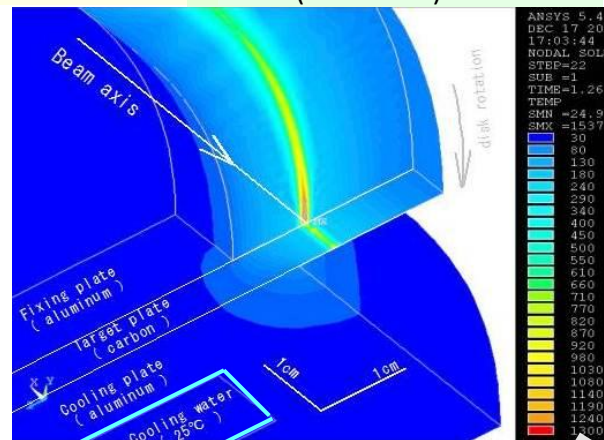
Be 15mm



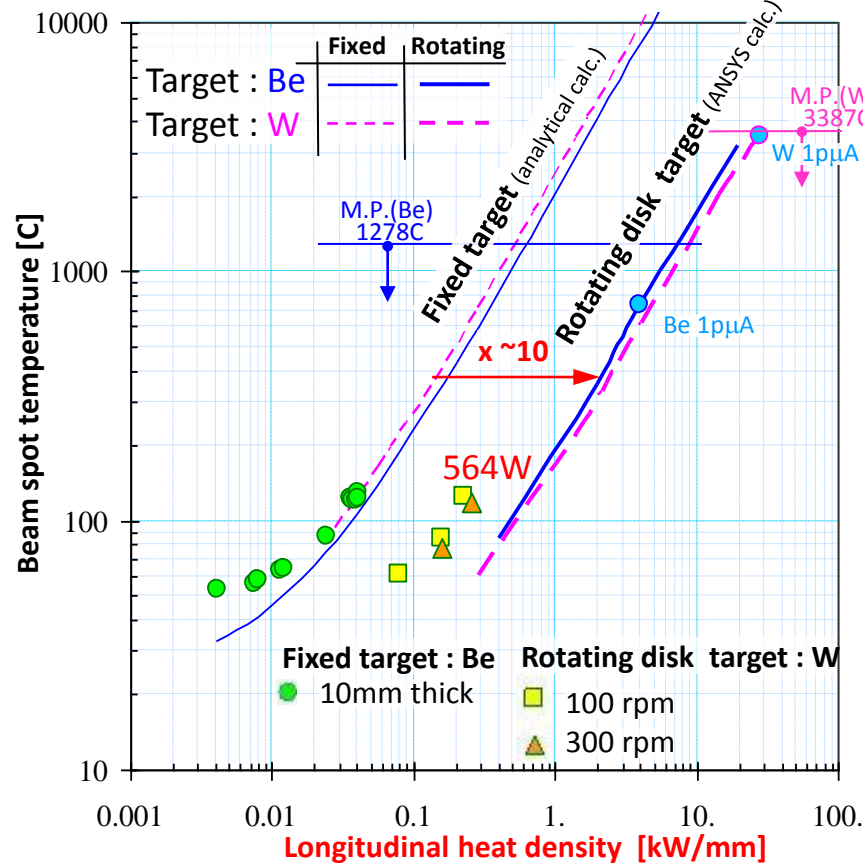
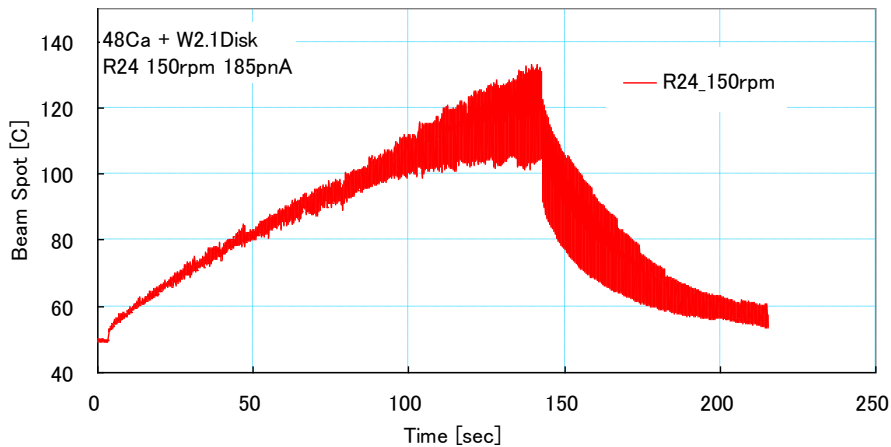
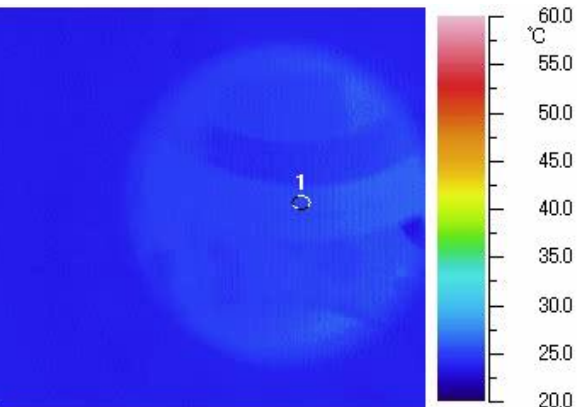
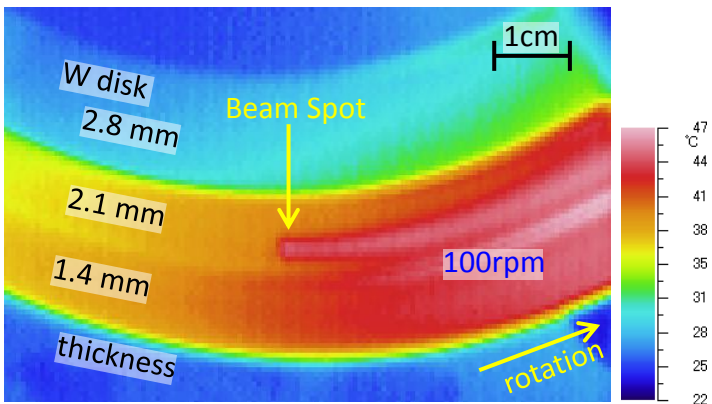
Rotating disk target ; temperature data

ANSYS (FEM code) simulation

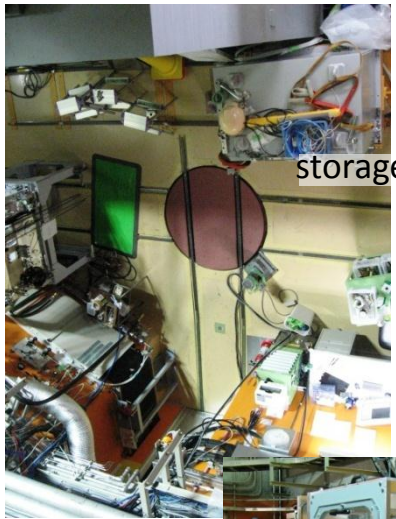
R024) W 2.1mm Disk 150rpm 185pnA (564W)



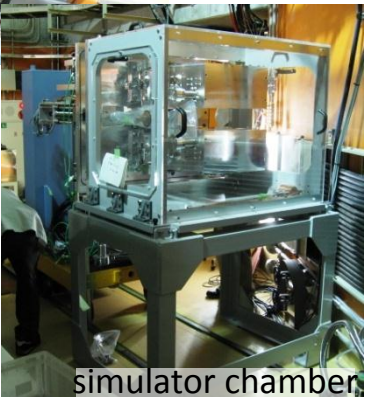
Calculation was made by A. Yoshida.



Target maintenance system



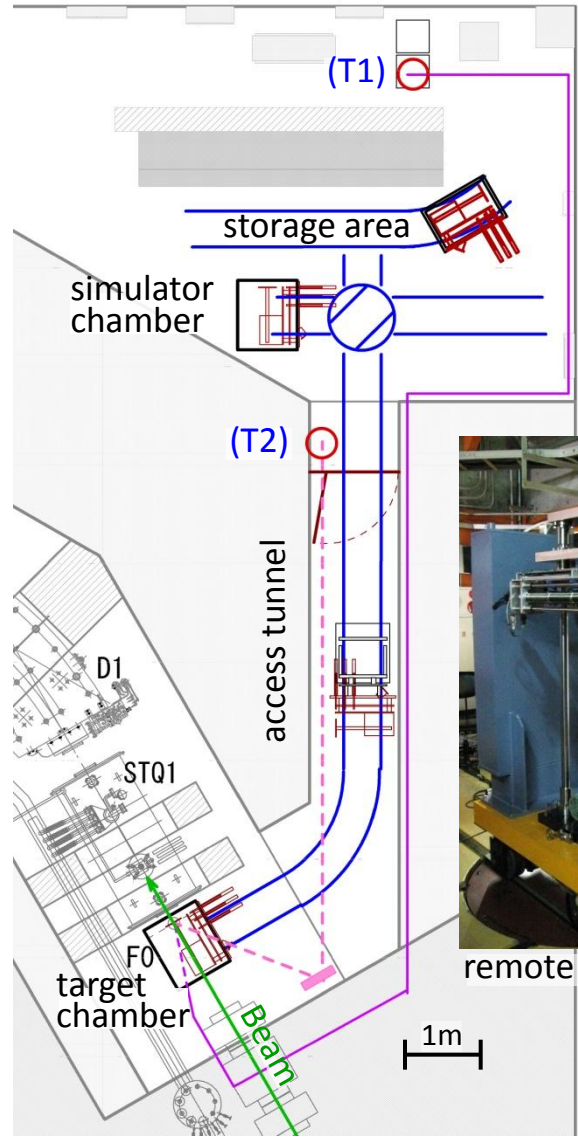
storage area



simulator chamber



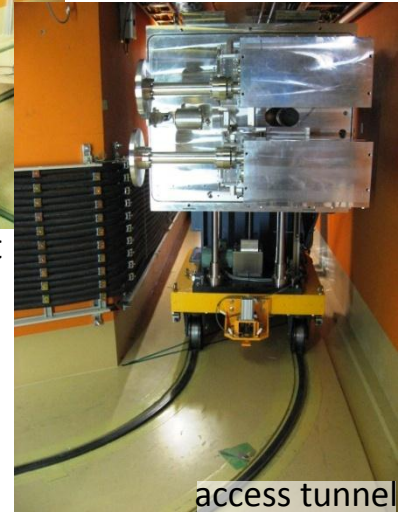
target chamber



storage cask



remote handling cart

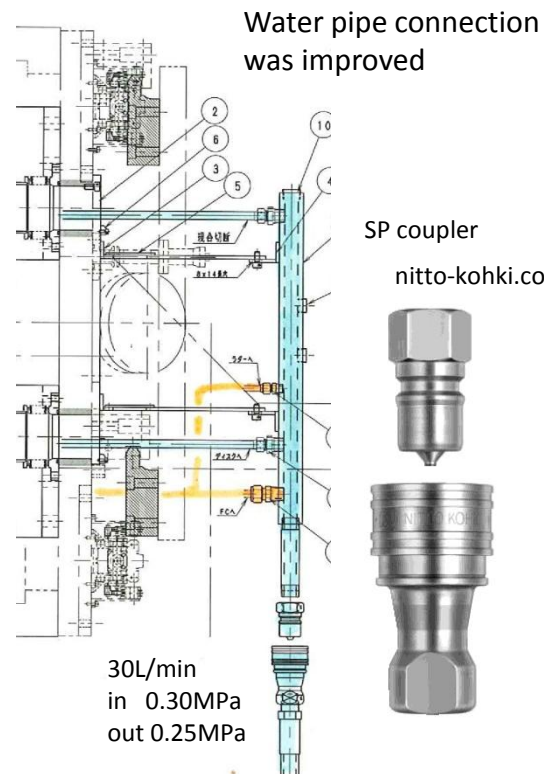
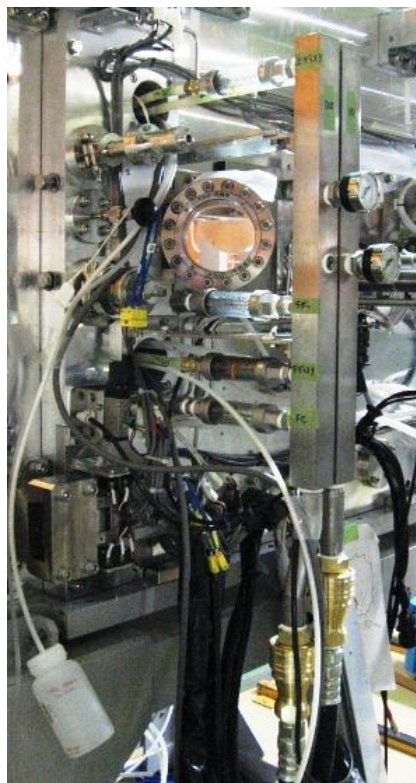
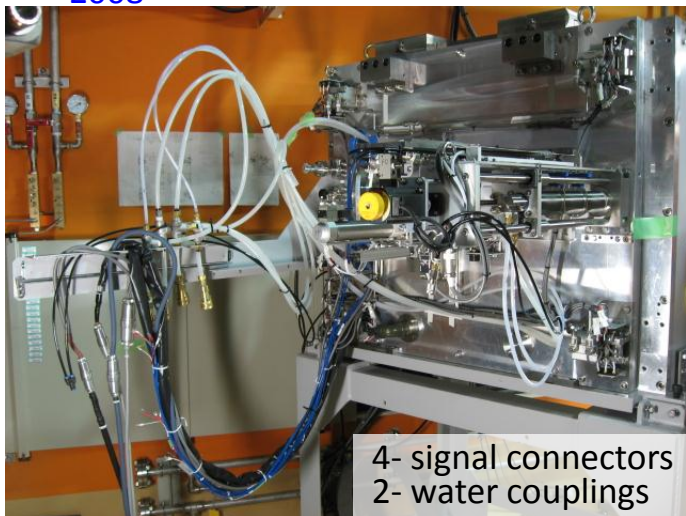


access tunnel

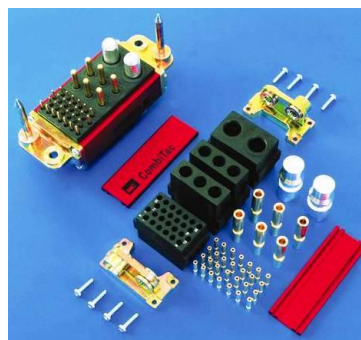
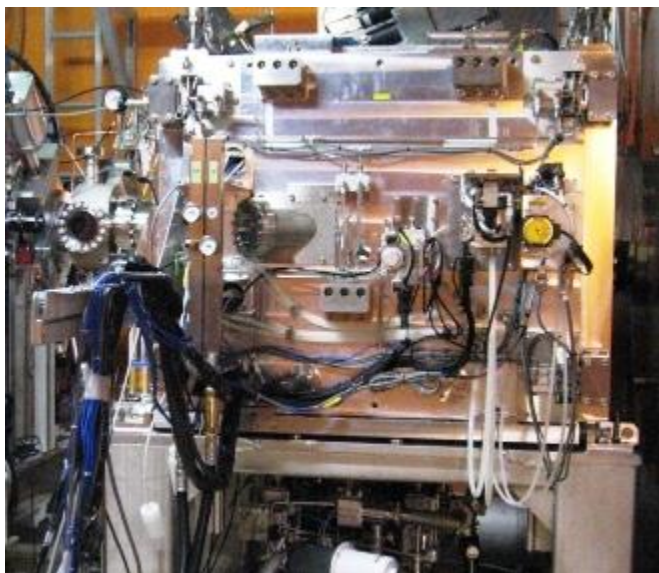
beam spot temperature monitors
 (T1) an infrared fiberscope
 (T2) infrared thermal camera

Cable connections at Removable flange unit

2008



2010



Power & signal cables:
Multi-contact connector

Multi-Contact **MC**
CombiTac STÄUBLI GROUP
multi-contact-usa.com

Summary

- The target system and the beam dump system which cope with ^{238}U 1pμA beam (83kW) have been designed and constructed. Features are described.
- The target and beam dump are operated without severe trouble although available beam intensity is less than 1/10 of goal intensity.
- Evaluations of the temperature of target and beam dump at a current beam intensity are important to prove the thermal performance of the target and the beam dump at the high beam intensity.
- Improvement of the maintenance system is progressing .