

## Introduction

- Muon colliders offer enormous potential for research of the particle physics frontier. Leptons can be accelerated without suffering large synchrotron radiation losses.
- In the core of the **Muon Collider facility** lays a **MW class production target**, which will absorb a high power (**1 to 3 MW**) proton beam to **produce muons** via pion decay.
- The target must withstand **high dynamic thermal loads** induced by 2 ns pulses at 5-50 Hz. Also, **operational reliability** must be guaranteed to reduce target exchanges to a minimum.
- **Different target technologies** with different levels of technological maturity are being explored.
- **An overview of the different target technologies** is presented, as well as details about the **target-systems engineering design for a C-Target option**.

## Pb-Liquid Target

### Opportunities

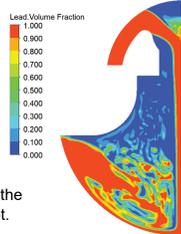
- **Known liquid-Pb / LBE thermo-hydraulics**
- **Cooling** outside vacuum chamber.
- **Radioisotopes** mostly retained.
- **No degradation** of target material.
- **Synergies** between different projects at CERN such as FCCee.

### Challenges

- Liquid-Pb containment **vessel and windows** (material, temperatures, DPA).
- **MHD** interaction.
- Cavitation-induced **erosion**.
- **Temperature and dynamic effects**.
- Dynamic multi-phase flow **simulation complexity**.

### Conceptual designs

- Pipe flow.
- **Vertical curtain**.
- Jet stream.

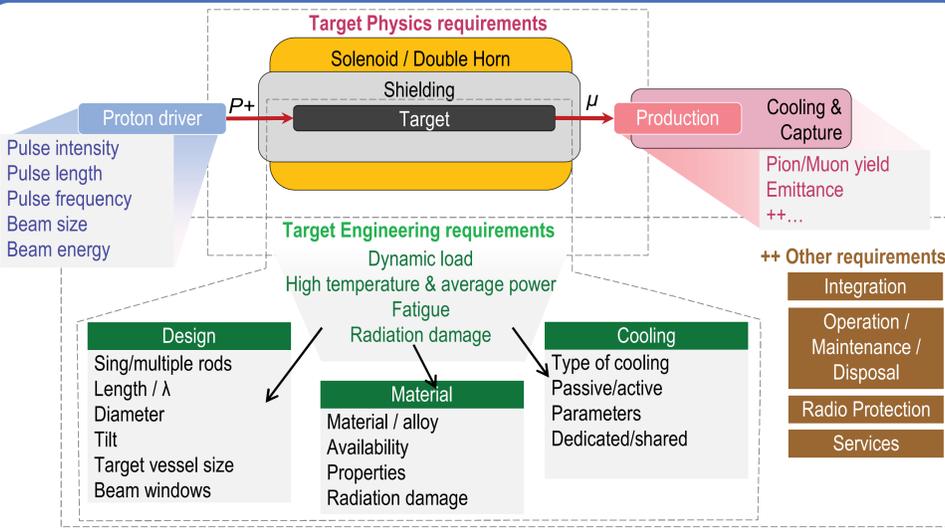


CFD modelling of the Pb curtain concept.

## Fluka Monte Carlo & Thermodynamic Parametric Analysis

- Parametric study on **beam sigma** and **pulse frequency**.
- Rod radius kept proportional to three times the beam sigma.
- Considered the **worst-case scenario**: only radiation cooling (No natural convection around the target).

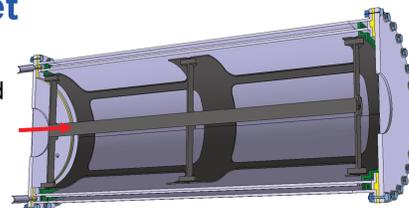
Proton driver beam parameters				
Parameter	Symbol	Unit	Baseline	Range
Beam power	$P$	MW	2	1.5 - 3.0
Beam energy	$E_{target}$	GeV	5	2 - 10
Pulse frequency	-	Hz	5	5 - 50
Pulse intensity	$n_p$	$10^{14}$ protons	5	3.7 - 7.5
Bunches per pulse	-	Number	1	1
Pulse length	$\sigma_z$	ns	2	1 - 2
Beam size	$\sigma_x$	mm	5	1 - 15
Impinging angle	-	degree	0.0	0.0 - 10



## C-Target

### Target Concept

- **Based on the CNGS target**, which operated up to 520 kW but could operate up to 750 kW.
- **80 cm isostatic graphite rod** (1.79 nuclear inelastic scattering lengths).
- Internal **Titanium vessel filled with static helium** (1 bar) to enhance natural convection and minimize graphite sublimation.
- Cooling water flowing between internal and external vessel.
- **Water cooled tungsten shielding**.
- The whole assembly will be surrounded by a superconductive solenoid.

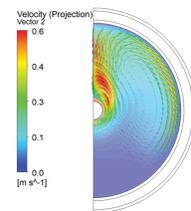


T peak (°C)	Transient				Steady state Average	Power deposited (W)
	5 Hz	10 Hz	20 Hz	50 Hz		
1	4301	3908	3735	3641	3583	44832
2	3318	3221	3177	3152	3135	59000
5	2740	2721	2713	2708	2704	90632
10	2305	2297	2293	2290	2288	129207
15	1947	1943	1940	1938	1938	163214

Maximum temperature and power deposition for 1.5 MW as function of the beam sigma. Thermal simulations run in ANSYS Mechanical for a radiation-only cooled target (No natural convection around the target).

### Cooling assessment via CFD

- Cooling & design optimization via CFD.
- Target vessel cooled by Helium at 3 m/s.
- Heat from graphite diffused by radiation + natural convection.

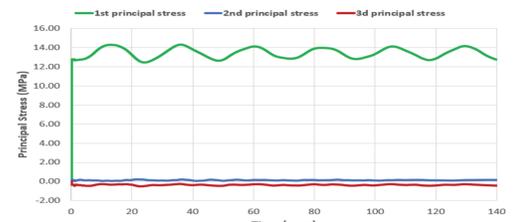


Principal stresses over time, which result following a single beam impact from a steady state initial condition. (At the most stressed point).

CFD computation of the static helium natural convection inside the target vessel.

### Dynamic response

- Case assessed: **sigma = 5 mm / 5Hz**.
- Maximum **energy density**: 173 J/cm<sup>3</sup>/pulse.
- Natural convection and radiation cooling considered.
- Dynamic stress waves assessed through the **explicit thermo-mechanical solver LS-Dyna**.
- Acceptable response due to large beam sigma and reduced interaction length.



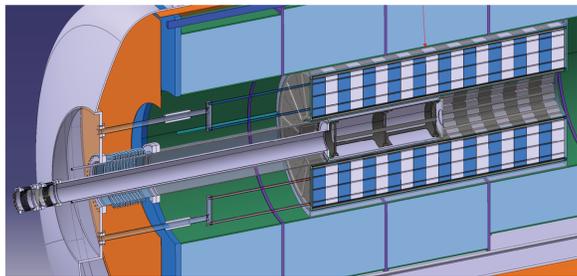
### Beam windows

- **Location**: p+ window outside cryostat assembly for better accessibility (maintenance, replacement, etc).
- **Fatigue**: extensive load cycles to be experienced by the target & windows (10<sup>8</sup>/y) at very high temperature.
- **DPA**: radiation damage may reach high values (>1 dpa) depending on material.
- **High power deposition**: e.g. 50-650 W (0.1 - 1 mm) for Titanium.
- **Possible strategies**: windowless, blown-up beam somewhere upstream, dual bunch, rotating window "dilution", frequent window exchange.

Double window concept cooled with helium

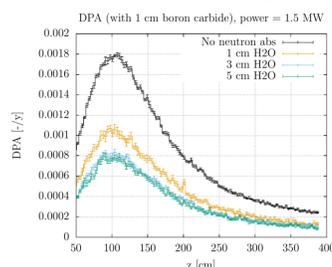


## C-Target systems



### Shielding design

- **Tungsten** shielding (23 tonnes).
- Most of the **thermal energy** is deposited on the shielding (34 %). The energy deposited on the target is 5.6 %.
- Donut + Pie blocks due to manufacturing limitations & to ease assembling.
- Longitudinal slots for locking & alignment pins.
- Helium cooled.
- Inner holes for bulk cooling. Inlet plenum for flow distribution.
- Outer layer with Boron carbide and H<sub>2</sub>O moderator.
- Routing and integration challenging inside SC Solenoid cryostat.

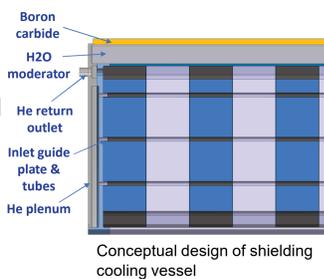
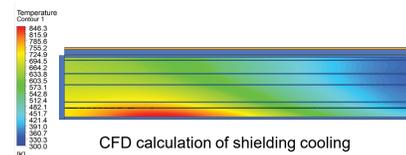


### Shielding optimization

- With neutron absorber, DPA reaches values of  $8 \times 10^{-4}$  DPA after 1 year.
- However, due to less W the Ionizing dose increases: >70 MGy after 10 years (3 cm H<sub>2</sub>O).

### Shielding cooling assessment

- Numerical analytical code to run across different parameters (flow, pressure, dimensions) to choose optimum operational point.
- Subsequent CFD calculation.



Conceptual design of shielding cooling vessel

## Conclusions

- Three different target concepts being explored. C-Target is baseline option and being used for the Front-hand target systems conceptual design and physics optimization.
- Heavy liquid metal target and a W fluidized target concepts are also being explored. Presenting a promising technological prospect for a 3-4 MW Muon Collider facility.
- In parallel to the target developments, the surrounding systems (shielding, beam windows and other) are being studied.