

Target and cooling system for the high intensity neutrino beams at J-PARC

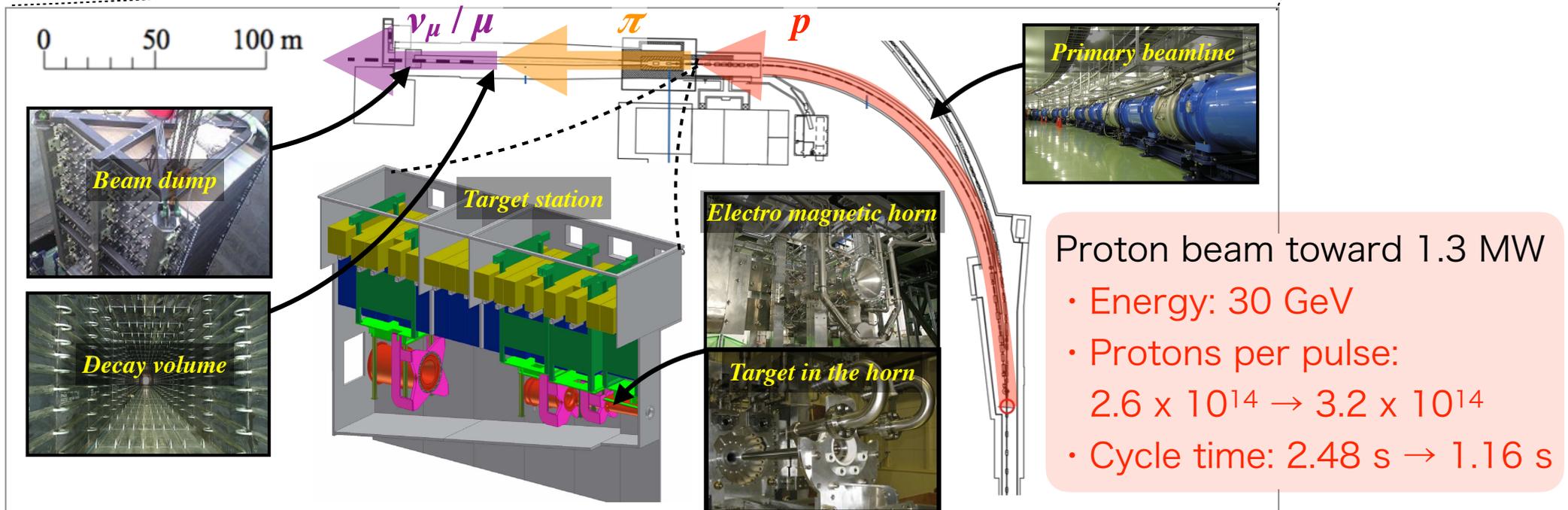
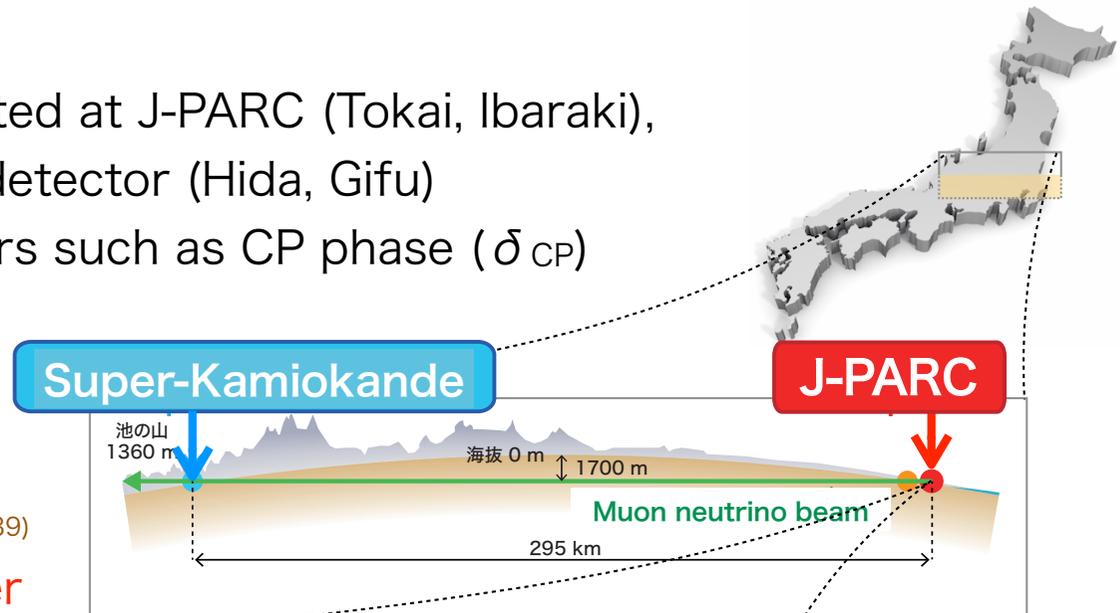
10 November 2023

Tsunayuki Matsubara (KEK/J-PARC)

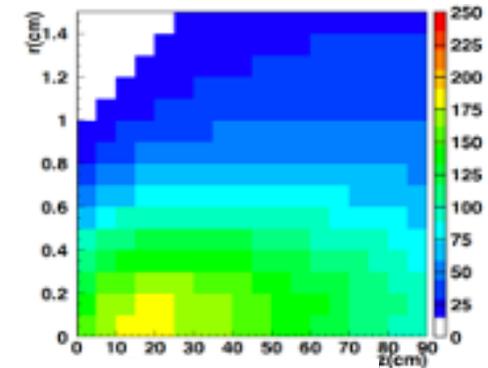
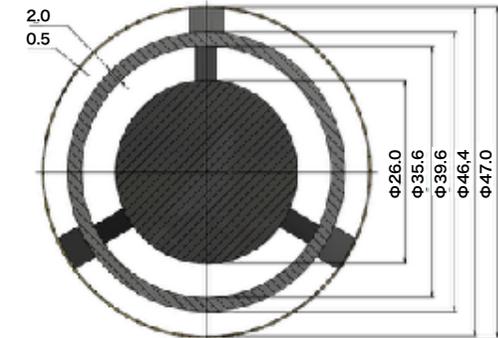
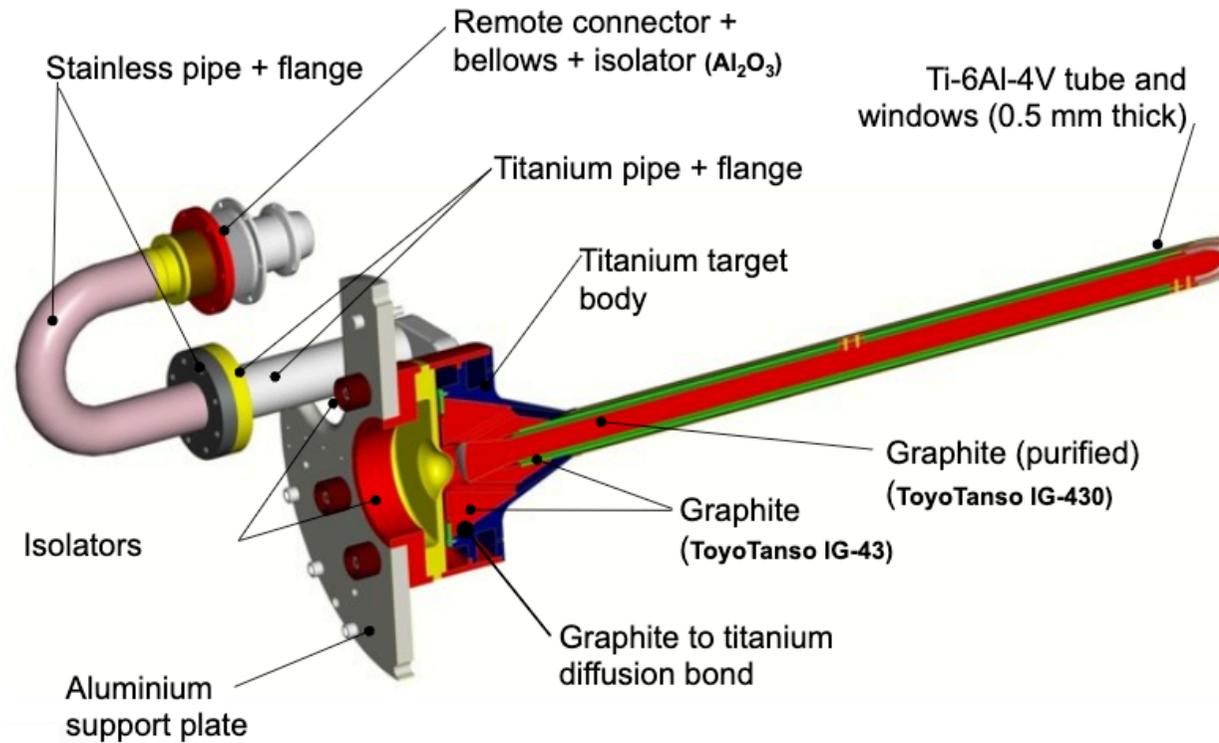
T2K experiment & ν beamline at J-PARC

High-intensity $\nu_\mu/\bar{\nu}_\mu$ beams are generated at J-PARC (Tokai, Ibaraki), and observed at the Super-Kamiokande detector (Hida, Gifu) to measure neutrino oscillation parameters such as CP phase (δ_{CP})

Showing the strongest δ_{CP} constraint w/ a hint of CP violation at $\sim 90\%$ C.L. using ~ 500 kW beam power (Nature 580 (2020) 339)
→ More statistics w/ 1.3 MW beam power



T2K Target - design concept

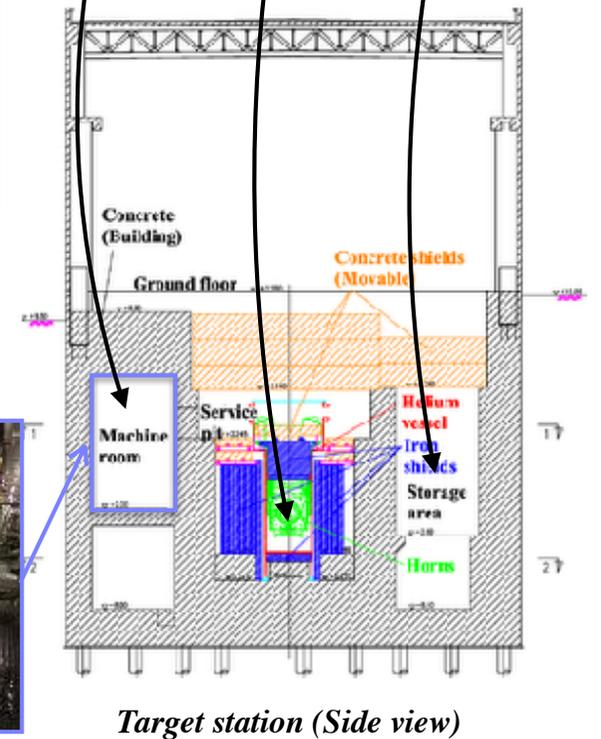
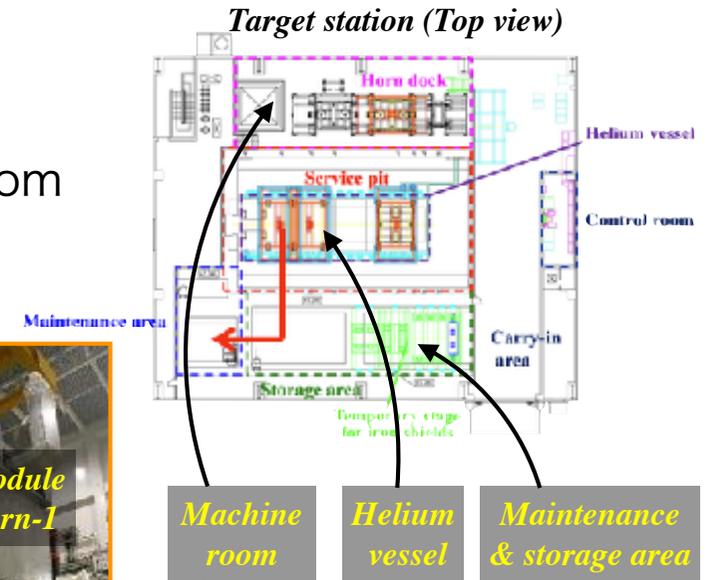
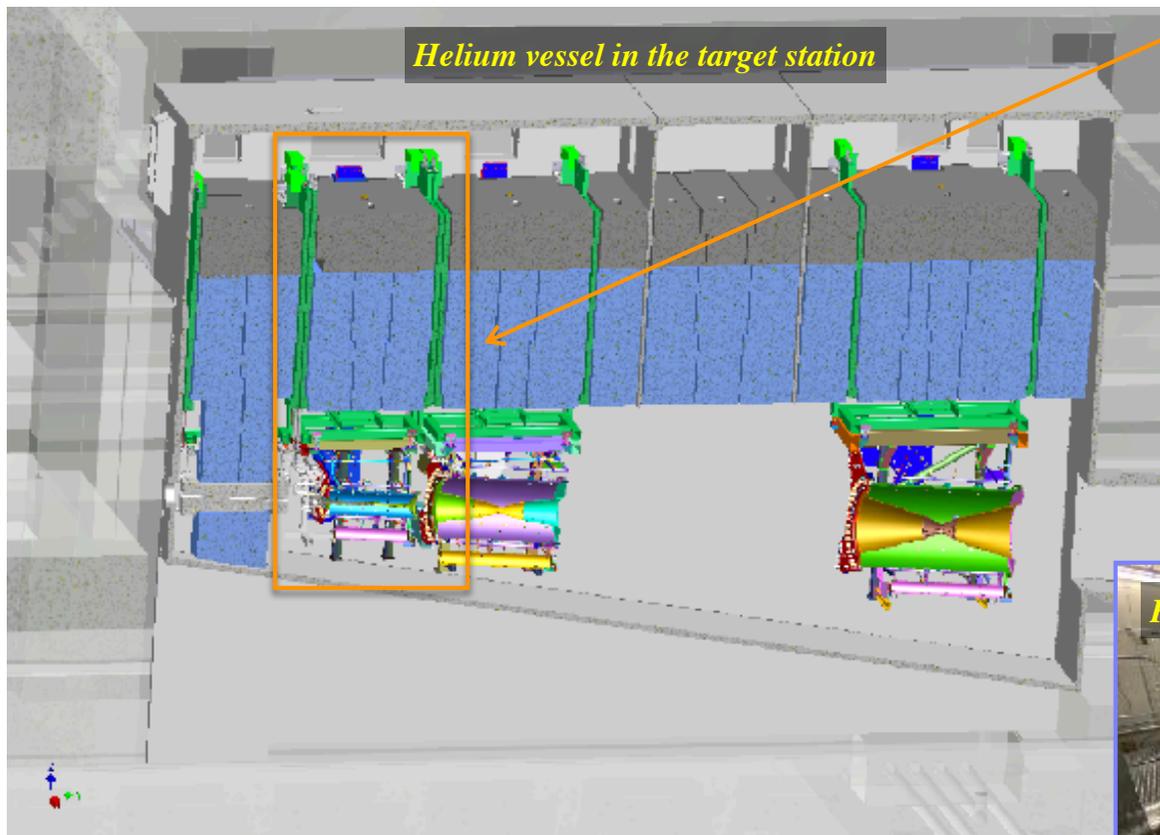


Simulated energy deposition (J/g/pulse)
for proton beam (3.3×10^{14} ppp)

- Isotropic graphite
 - Low density for low heat generation density. Thermal shock tolerance. Radiation hardness
- ~90 cm long ($\sim 2 X_0$) & 26 mm Φ ($\sigma_{\text{beam}} = \sim 4.2$ mm) → Maximizing pion yield
- Cantilever → To accept graphite shrinkage
- Co-axial two pipes, Ti-alloy (Ti-6Al-4V) container, up/downstream window
 - For single side Helium gas cooling from upstream
- He cooled
 - To minimize pion absorption. To avoid heat generation of refrigerant.
 - To all higher operating temperature (above 400°C to reduce radiation damage in graphite)

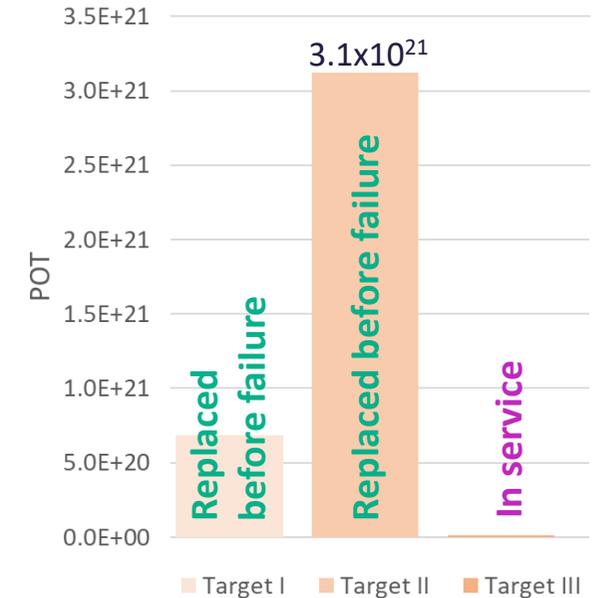
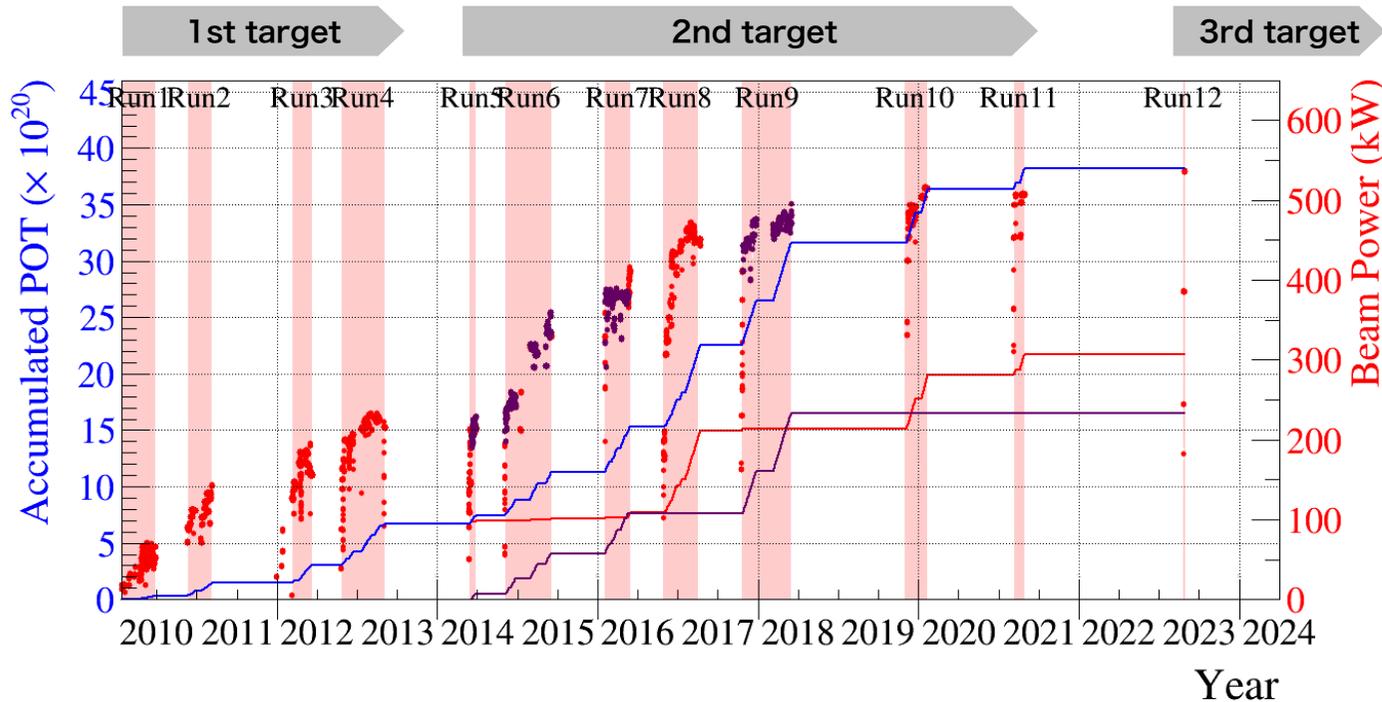
Layout of the target & cooling system

- Target installed inside Horn-1 in the Helium vessel
- Helium compressor for cooling is located at the machine room
- Remote exchange is conducted in the maintenance area



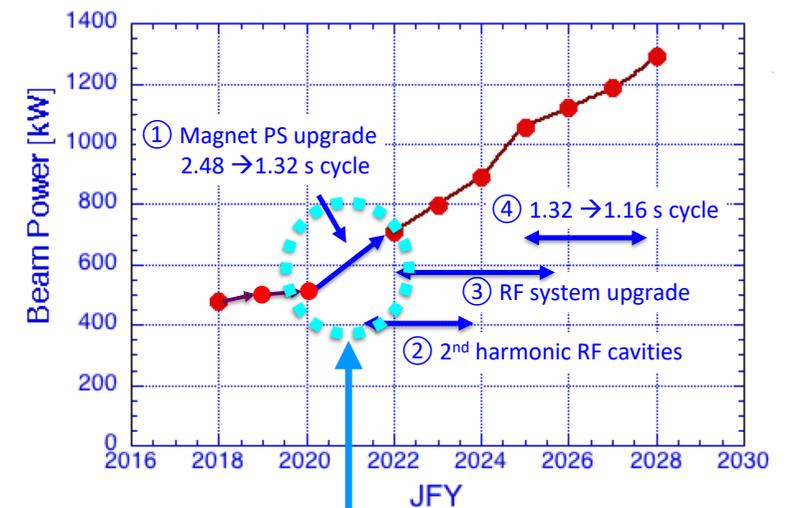
Operation history and future

(*) POT: Proton on target



Exposed POT for each target

	1st target	2nd target	3rd target
Period	09' Apr. ~ 13' May	14' Nov. ~ 21' Apr.	22 Apr. ~
POT	0.7×10^{21}	3.1×10^{21}	0.01×10^{21}
Max. beam power	~230 kW	~490 kW	~540 kW
Comment	<ul style="list-style-type: none"> No significant trouble Replaced with horn-1 	<ul style="list-style-type: none"> He leak at ceramic part and fixed in 15' Replaced with horn-1 	<ul style="list-style-type: none"> To be remotely exchanged in 25' for 1.3 MW

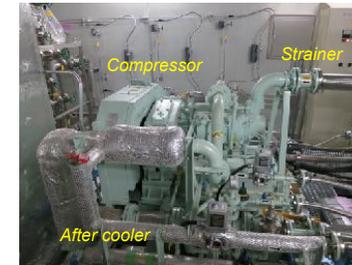
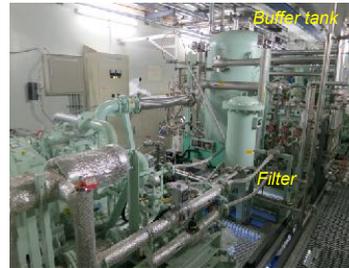


Long shutdown in 21'/22'

Neutrino event rate (POT normalized) monitored by T2K near detector is stable so far → Target is fine

Current Helium gas cooling system

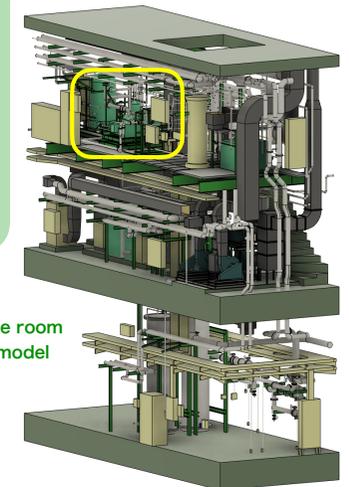
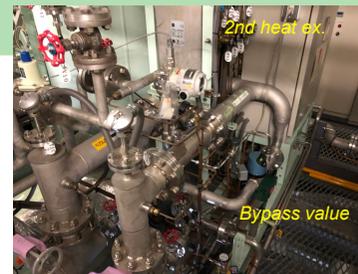
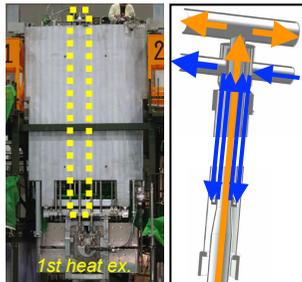
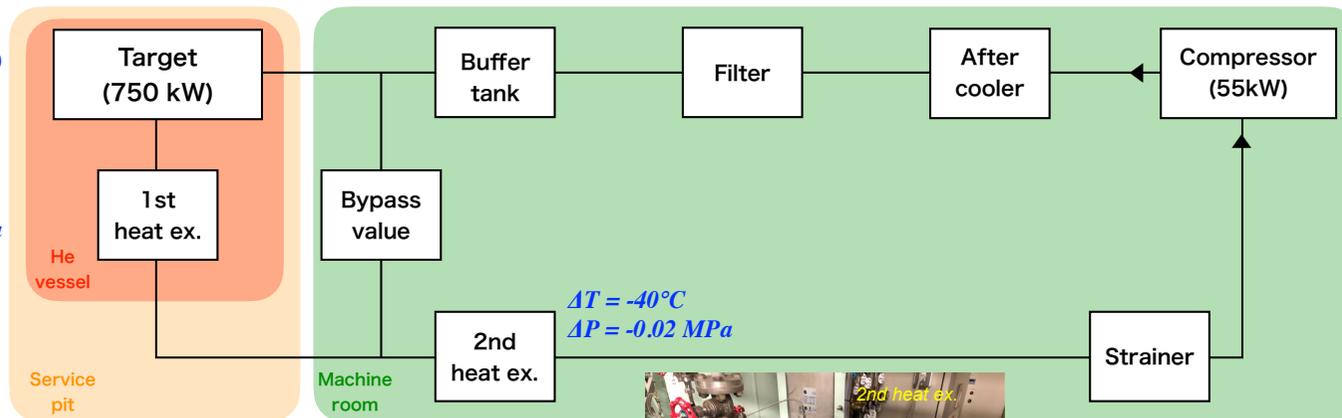
Current target cooling capacity : 750kW + 20% margin = 900 kW (Beamline upgrade TDR: arXiv:1908.05141)



$T = 200^{\circ}\text{C}$ ($\Delta T = 170^{\circ}\text{C}$)
 $\Delta P = -0.07 \text{ MPa}$

$\Delta T = -130^{\circ}\text{C}$
 $\Delta P = -0.06 \text{ MPa}$

$T = 30^{\circ}\text{C}$
 $P = 0.16 \text{ MPaG}$
 $Q = 660 \text{ Nm}^3/\text{h (Max)}$

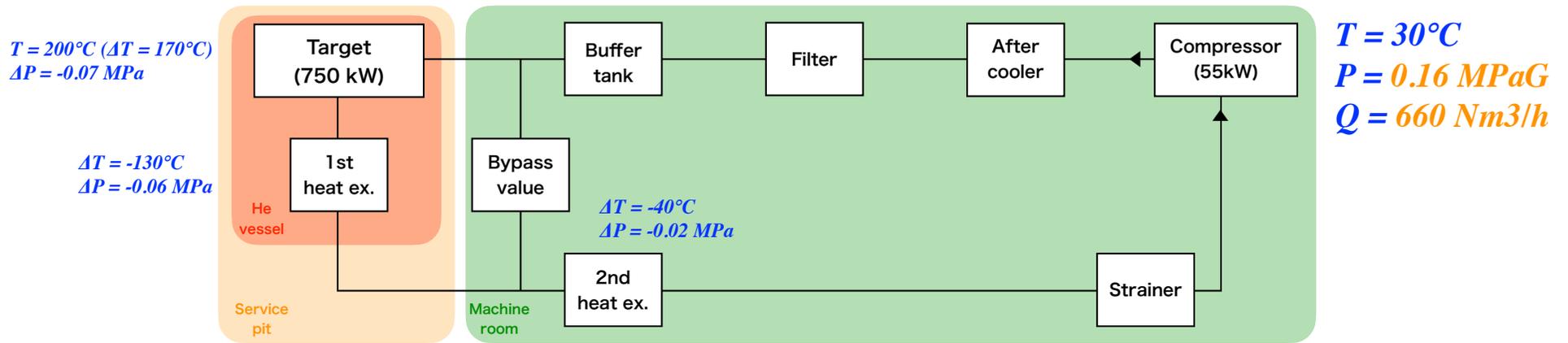


- Need to have doubled mass flow rate, i.e. 32 g/s (660 Nm³/h) → 60 g/s (1200 Nm³/h), but we can not just increase flow rate due to pressure drop and Helium velocity
→ Increase operating pressure

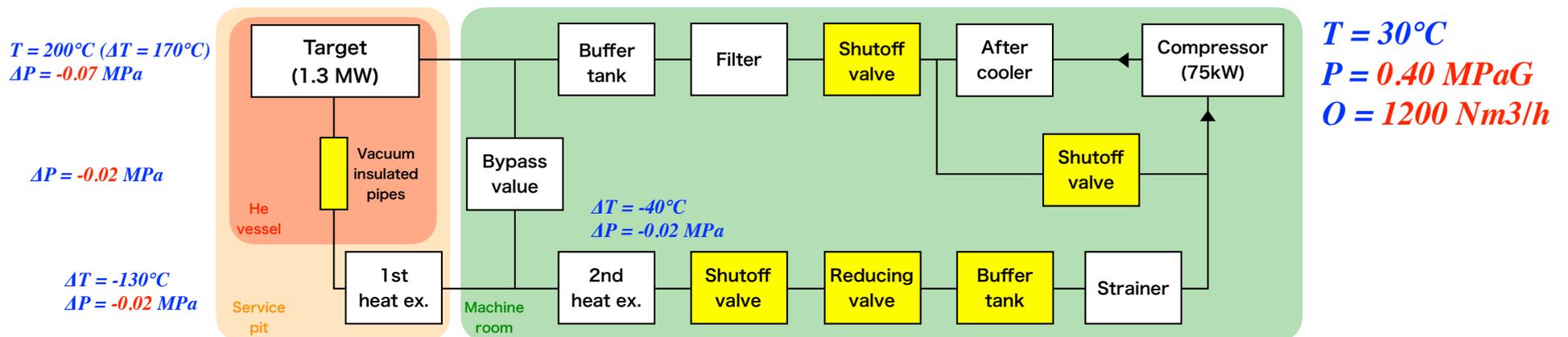
Upgrade to increase operating pressure

- All components to be renewed for the high pressure tolerance/operation by 2025
e.g. 1st heat exchanger pipe was exchanged to vacuum insulated pipes + heat exchanger

Before upgrade



After upgrade

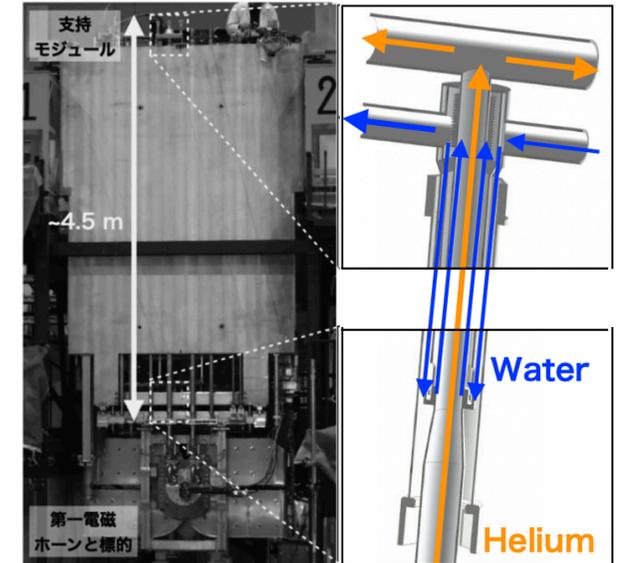


New components in the machine room to be installed in 25'

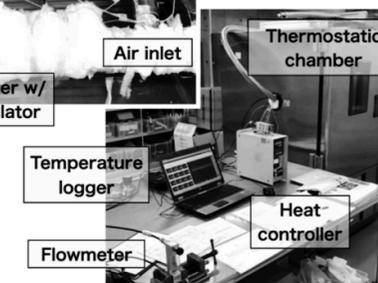
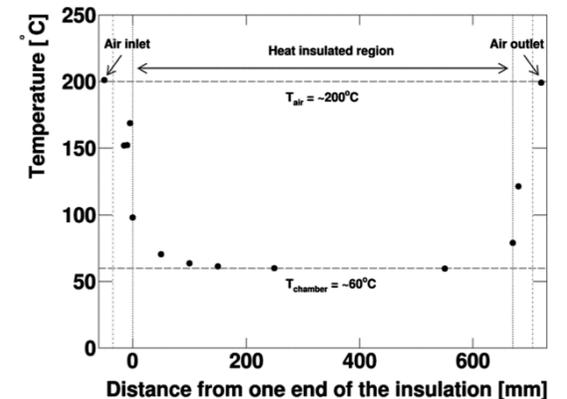
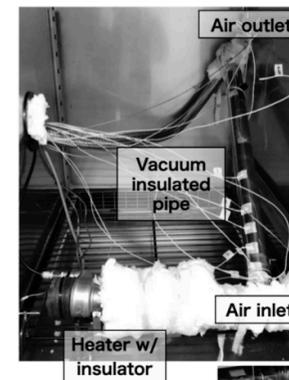
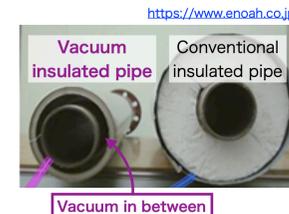
- Shut off vales : For star-delta starter (reduced current but no load operation required)
- Reducing valve : Required to protect compressor inlet ($< 0.4 \text{ MPaG}$)
- Buffer tank : Required to have reduced filling pressure ($\sim 0.3 \text{ MPaG}$)

Challenges to exchange the 1st heat exchanger

- The original first heat exchanger in the support module
 - Pipes & bellows rated up to 0.2 MPaG operation
 - Need to replace
 - Water cooled with cylindrical structure (gas, water, water, wrench)
 - Large pressure drop due to small inner diameter ($\phi 23.9$)
 - $\phi 65$ outer diameter in $\phi 70$ hole in the radioactive steel plate
 - Constraint of mechanics & radiation
 - Located in the Helium vessel
 - Difficult to maintain. Tritium production in water

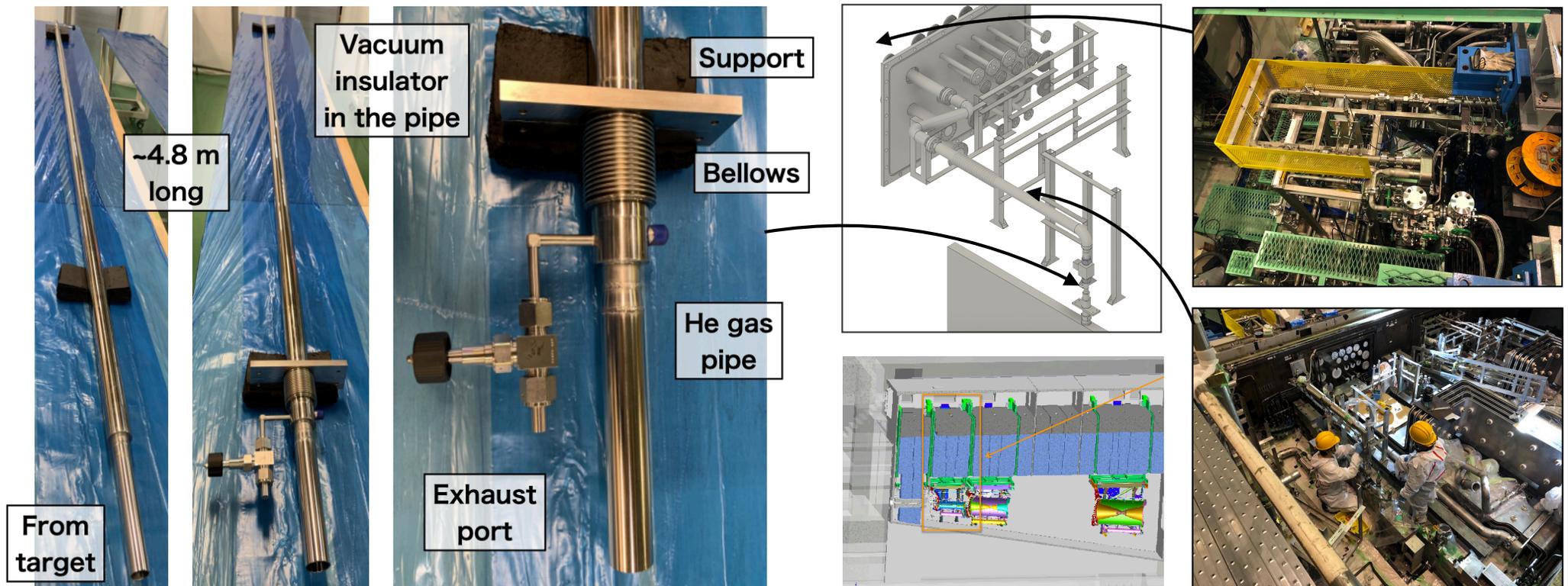


- Developed new scheme w/ vacuum insulated pipe
 - Higher pressure tolerance
 - Enlarged diameter ($\phi 23.9 \rightarrow \phi 30.7$) for low ΔP
 - New heat ex. at outside Helium vessel
- Produced small prototype
 - Tested with a air with heater in a chamber
 - Showed an excellent insulation performance



Upgrade work in the last long shutdown

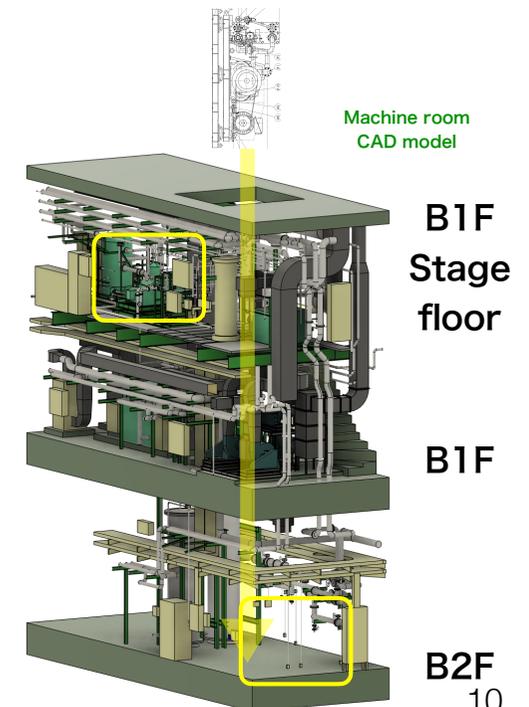
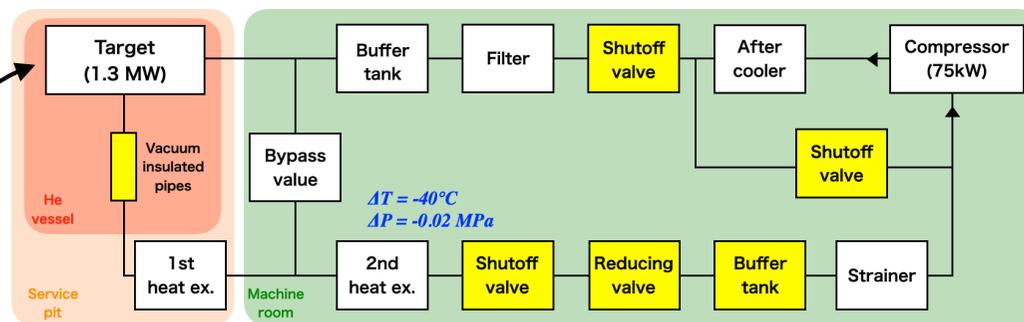
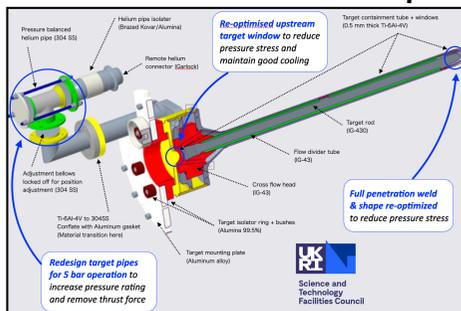
- Produced new insulated pipe with 4.8 m long & other 3 pipes in the Helium vessel
- Dismantled the old 1st heat exchanger by cutting top part (less radiated)
- Install new pipes with other upgrade works like horn and target replacement
- Installed new heat exchanger outside Helium vessel



- Already confirmed insulation performance in the beam operation this year up to 540 kW

Plan to complete upgrade in 2025

- 1.3 MW target production well in progress (as presented by Mike on Tuesday)
- New compressor and filter unit for high outlet pressure (0.4 MPaG) was delivered
- Now developing the new circulation system to have commissioning work in 2024
- Making installation plan carefully to fit existing facility



Estimate of target oxidation by the He cooling gas

Question: How much carbon consumed by oxidation?

- Allowed target loss reduction by design is 2%,
i.e. ~17 g out of 869 g (target-rod mass)

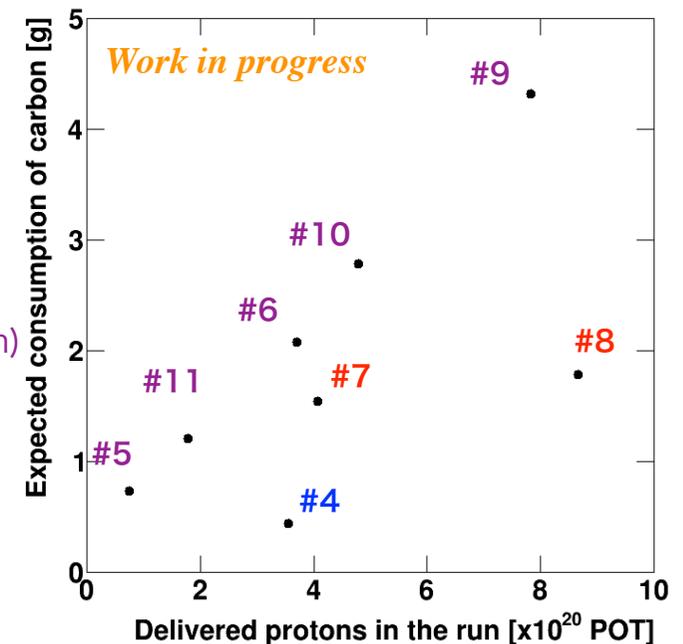
Gas impurity measurement of O₂, CO, CO₂, H₂, CH₄, N₂ by a gas chromatography system in the Target station

- System based on GC2014 (SHIMAZU CORPORATION)
- Operating since 2013 (in the middle of Run #4)
- Before beam operation, high purity He gas is filled, targeting to control O₂ contamination with ~1 ppm

Oxidation is estimated from CH₄, CO, CO₂ contamination after the beam operation

- ~2% loss after $\sim 3 \times 10^{21}$ POT (equal to 1.3 MW x 6 months operation)
if we ignore outliers and assume naive extrapolation
- Overestimating? Carbon may come from other parts like a slider of the compressor.

To be checked with more data with a high repetition rate



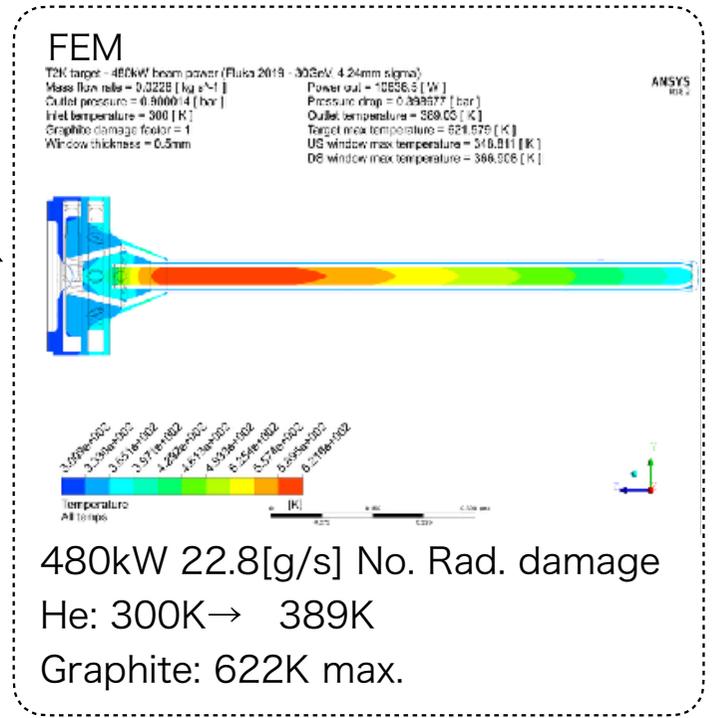
Summary

- Target and cooling system for the T2K experiment is in operation since 2009, accumulating experiences for the high intensity neutrino beams at J-PARC
- Beam power upgrades beyond original design requires replacement of the target and cooling system to increase operating pressure of He cooling gas
- Upgrades of cooling system in progress. Vacuum insulated pipes were adopted to realize the high pressure tolerance and low pressure drop in a confined space
- Completion of the upgrade foreseen in 2025 after commissioning and installation of the new circulation system in the machine room
- Estimation of target oxidation from impurities in the He gas was performed. To be evaluated more in the future operation with the higher beam power

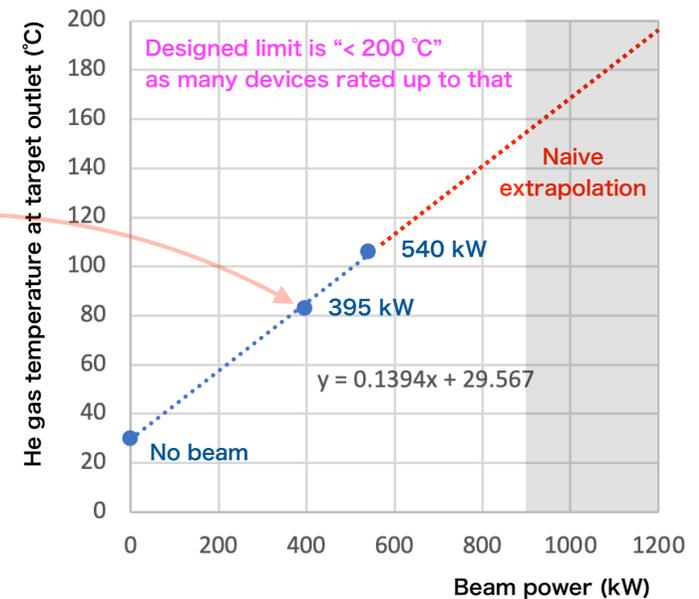
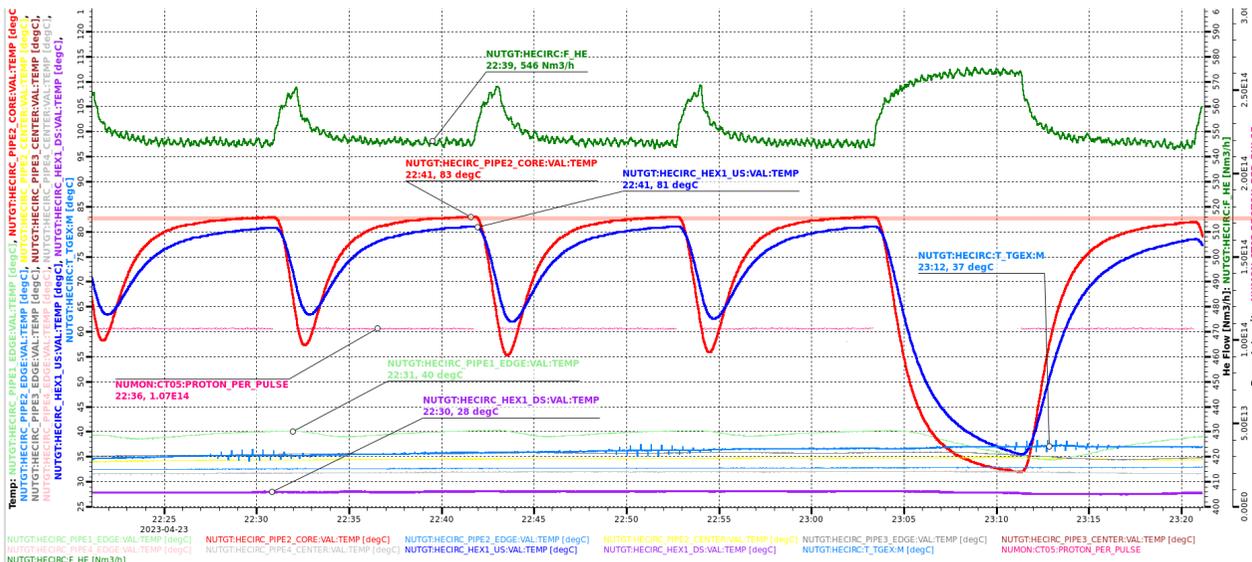
Backup

He gas measurement so far

- He gas temperature is measured during beam operation
 - 490 kW beam, He flow ~ 25 g/s → $\Delta T_{\text{Helium}} \sim 72\text{K}$
 - Latest simulation with FLUKA (2019) & ANSYS
 - 480 kW beam, He flow 23 g/s → $\Delta T_{\text{Helium}} \sim 89\text{K}$
 - (*) Simulated ~145K with MARS (2006)
- No significant discrepancy



NOTE: Naive explanation based on the latest measurement shows that we can increase the power beyond 900 kW before 25'. But we have to check it with larger power in the Nov./Dec. run. Some margin by He flow rate (550 Nm³/h), filling pressure (~0.17 MPaG).



An example of the latest monitor during 395 kW operation in 23' April (After replacement of the 1st heat exchanger)

Flow rate setting (discharge pressure, bypass opening rate & fill pressure)

How to adjust the flow rate in the current circulation system:

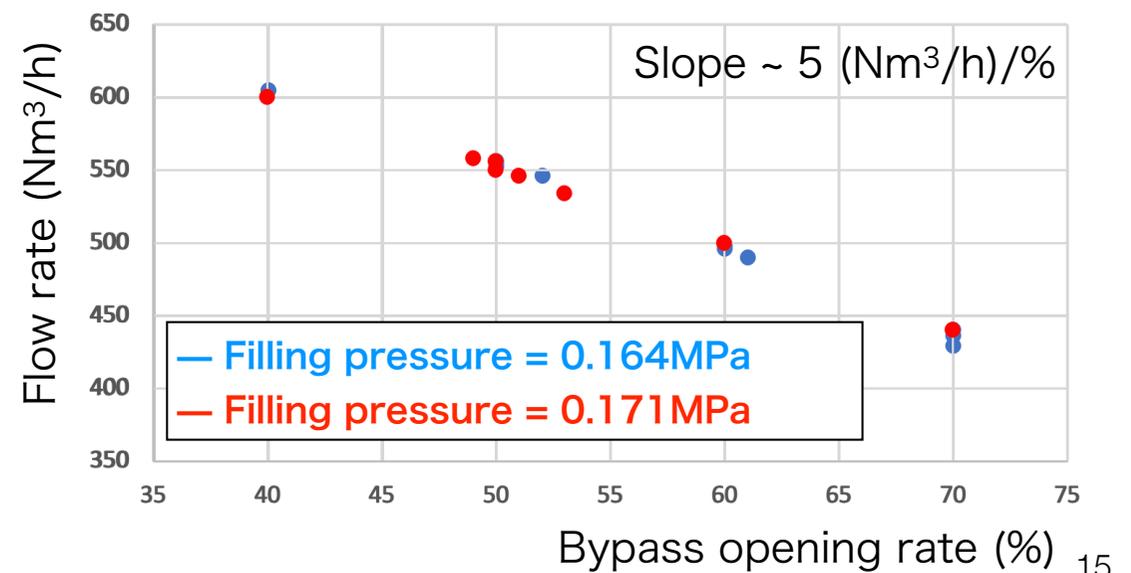
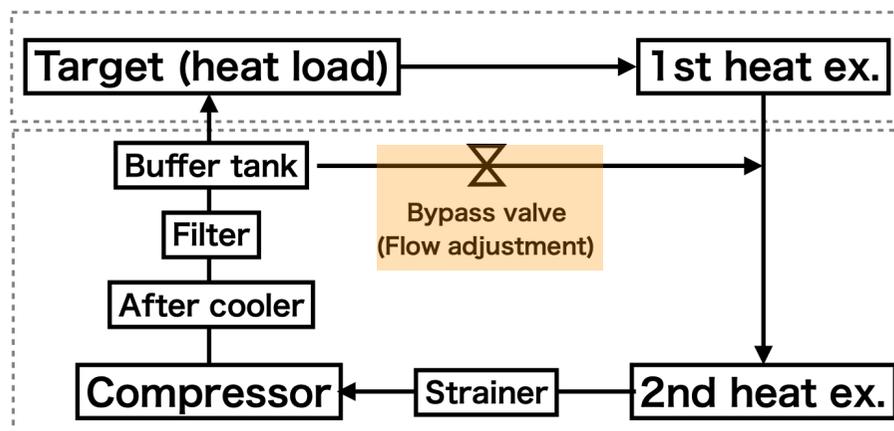
- 1) Set **discharge pressure** (e.g. 0.165 MPaG) of the Helium compressor
- 2) **Bypass opening rate** is changed (Automatic mode in [0, 100]%)
- 3) **Flow rate** changes accordingly

Checked **flow rate** varying **bypass opening rate** to know the optimal setting

→ Linear correlation between those

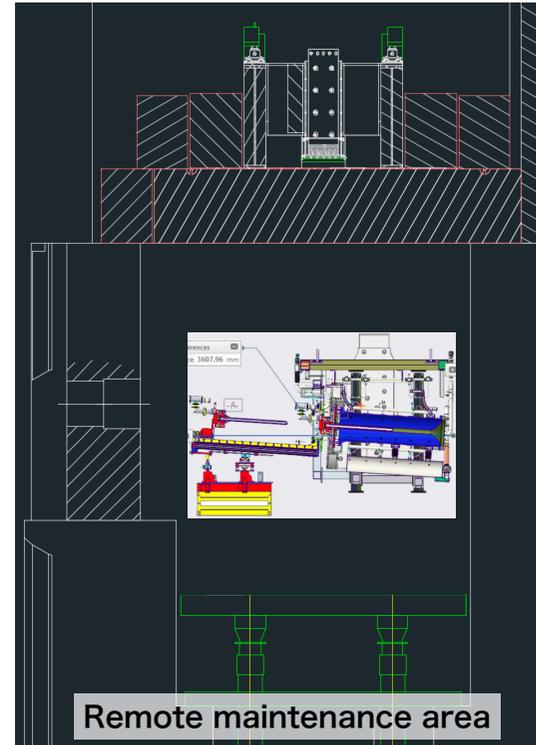
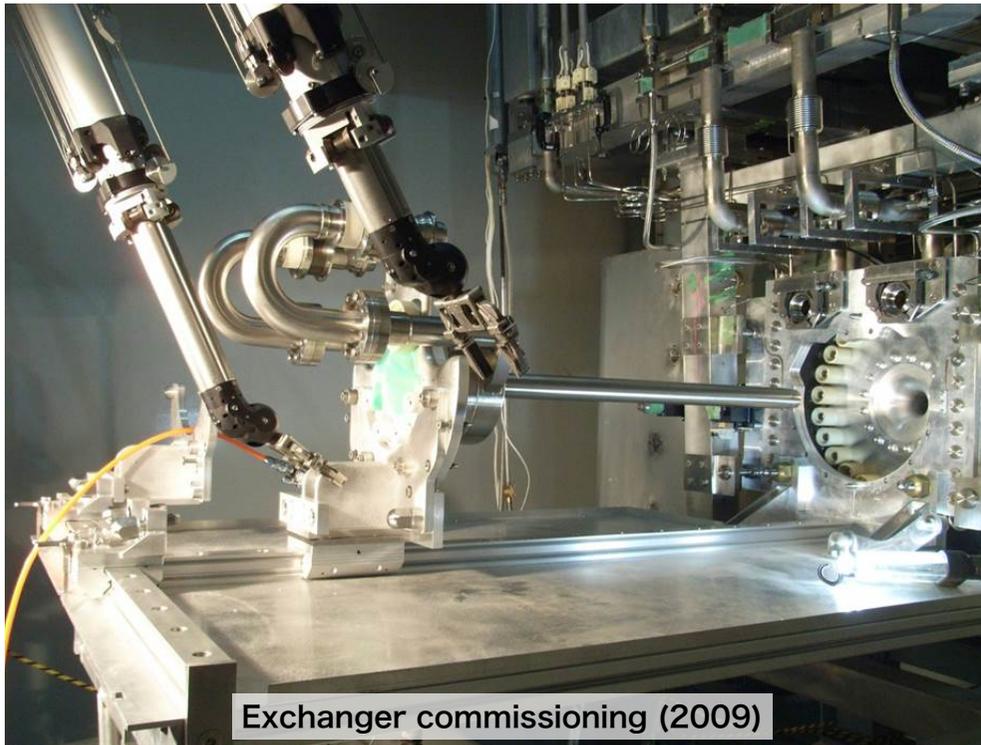
→ Not affected by **filling pressure** (unless it has sufficient pressure for discharge)

→ Decided appropriate settings to provide flow rate of 560 Nm³/h for 750kW



Target remote exchange

We will have to remove/install the targets remotely to the highly radioactive horn
 → This allows the large and expensive magnetic horn in which the target is installed to be reused, saving money and reducing radioactive waste.



Challenges to exchange targets :

- The clearance between the target and horn bore is only 3 mm
- Target is ~1 m long and contains delicate graphite components

→ Designed/developed a “remote exchange system” which permits targets to be safely and quickly replaced using master-slave manipulators in a remote maintenance area

Target exchanger

